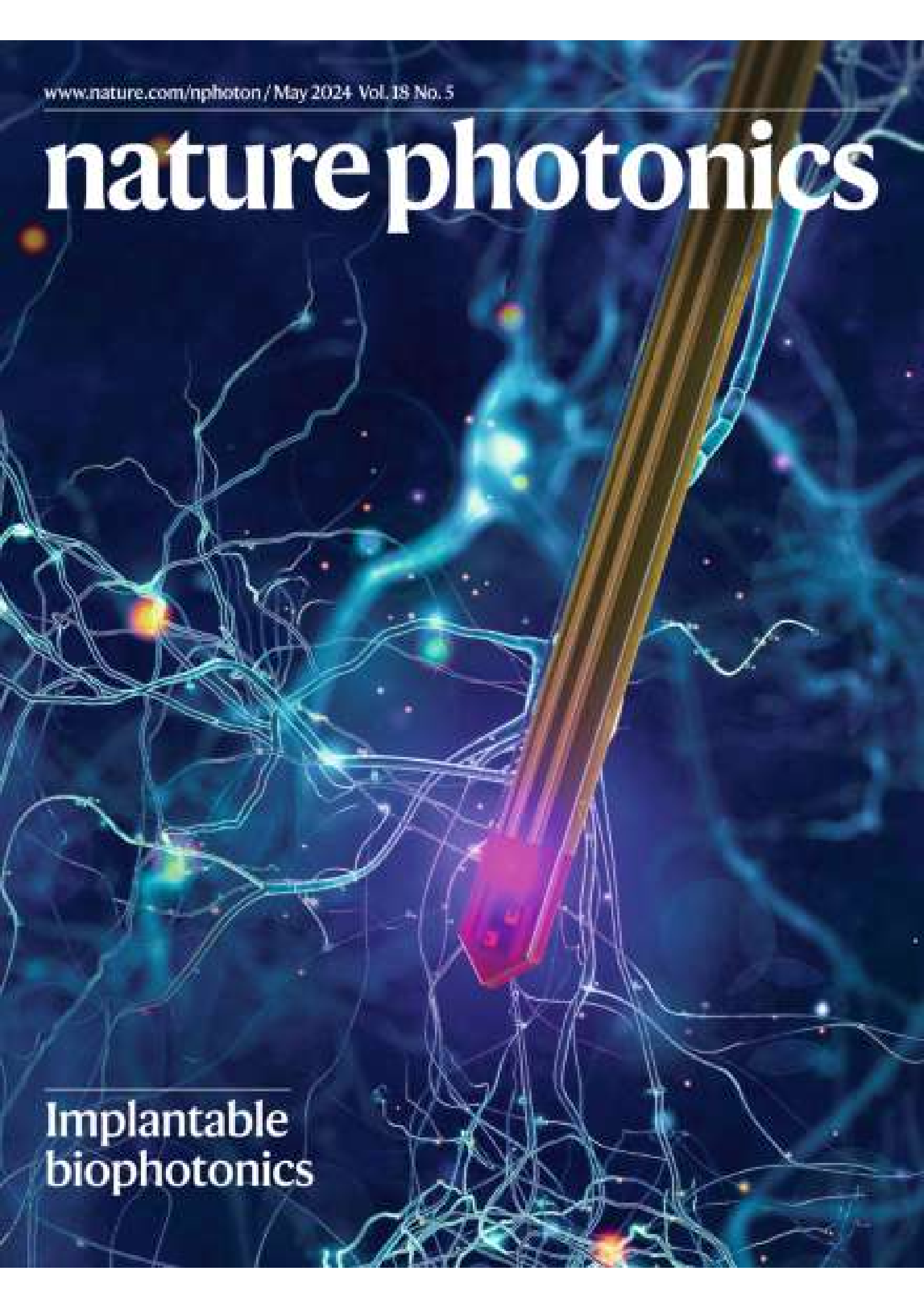


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# A wireless optoelectronic probe to monitor oxygenation in deep brain tissue

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Real-time detection of tissue oxygenation in the nervous system is crucial in neuroscience studies and clinical diagnostics. Complementary to blood oxygenation levels, the partial pressure of oxygen in brain tissue ( $p_{\text{btO}_2}$ ) plays a key role in regulating local neural activities and metabolism. Here we develop an implantable optoelectronic probe that wirelessly and continuously monitors  $p_{\text{btO}_2}$  signals in the deep brain of freely moving rodents. The thin-film, microscale implant integrates a light-emitting diode and a photodetector, and is coated with an oxygen-sensitive phosphorescent film. Powered by a battery or an inductive coil, a miniaturized circuit is capable of recording and wirelessly transmitting  $p_{\text{btO}_2}$  signals. The wireless micro-probe captures cerebral hypoxia states in mice in various scenarios, including altered inspired oxygen concentrations and acute ischaemia. In mouse models with seizures, the micro-probe associates temporal  $p_{\text{btO}_2}$  variations in multiple brain regions with electrical stimulations applied to the hippocampus. Our probe and method offer important insights into neuroscience studies regarding neurometabolic coupling and pave the way for the clinical application of implantable wireless optoelectronic probes.

The supply of oxygen ( $\text{O}_2$ ) is vital in human metabolism. Hypoxia, in which tissue oxygenation is below the normal level, can cause the dysfunction of, damage to and even the death of biological cells and organs<sup>1,2</sup>. As a leading consumer of  $\text{O}_2$ , the human brain, which constitutes only ~2% of the body weight, expends ~20% of the body's total  $\text{O}_2$  supply to continuously maintain its normal function<sup>3</sup>. Cerebral hypoxia, which is caused by acute brain abnormalities such as poisoning, traumatic brain injury and subarachnoid haemorrhage<sup>4–6</sup> or

diseases including hydrocephalus and brain tumours<sup>7,8</sup>, can lead to irreversible damage of the brain function and result in disability and death. In addition, cerebral hypoxia is closely associated with neurological and cerebrovascular diseases such as epilepsy and apoplexy, as well as various neurodegenerative disorders<sup>9,10</sup>. Therefore, real-time monitoring of the cerebral oxygenation state is crucial, not only for understanding the metabolic coupling between  $\text{O}_2$  and brain activities but also for improving clinical practices<sup>11,12</sup>.

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Conventional biological techniques that detect  $O_2$  in the brain mostly rely on near-infrared spectroscopy and functional magnetic resonance imaging<sup>13,14</sup>. Near-infrared spectroscopy, along with other recently reported invasive  $O_2$ -sensing probes<sup>15,16</sup>, assesses the cerebral blood oxygen saturation ( $S_{tO_2}$ ) by exploiting the difference in optical absorption between oxygenated and deoxygenated haemoglobin ( $HbO_2$  and  $Hb$ , respectively)<sup>17</sup>. Alternatively, blood-oxygen-level-dependent (or BOLD) imaging in functional magnetic resonance imaging focuses primarily on the concentration of  $Hb$  in the blood flow<sup>18</sup>. Whereas  $S_{tO_2}$  reflects the concentrations of  $Hb$  and  $HbO_2$  in the blood transported through the vessels, its value sometimes deviates from the partial pressure of  $O_2$  in brain tissue ( $p_{btO_2}$ )<sup>19</sup>. Non-invasive methods for direct  $p_{btO_2}$  detection involve electron paramagnetic resonance<sup>20</sup> and positron emission tomography<sup>21</sup>, which rely on injected or inhaled  $O_2$  tracers that delay the detection of  $p_{btO_2}$  and bulky, high-cost instruments that prohibit portable use.

To measure local  $p_{btO_2}$  signals, clinically available techniques utilize the insertion of electrochemical or optical probes into the targeted region. Electrochemical methods based on polarographic analyses use Clark-type electrodes or other conductive wires to detect  $p_{btO_2}$  signals via oxidative reactions<sup>22–25</sup>. These chemical electrodes typically consume  $O_2$  during detection, require a certain time to stabilize and are vulnerable to contamination from interfering substances in the absence of a carefully designed  $O_2$ -selective membrane<sup>25,26</sup>. Optical techniques leverage phosphorescent dyes whose luminescence efficiencies or lifetimes decay with the addition of  $O_2$  (ref. 27), so that the tissue oxygenation can be sensed via imaging or spectroscopic setups<sup>28,29</sup>. Compared with electrochemical probes, the luminescence quenching process exhibits superior  $O_2$  selectivity and promising resistance to electromagnetic interference<sup>3,29,30</sup>. Traditional tools based on this mechanism for the sensing of  $O_2$  utilize tethered fibre-optic systems for light delivery and collection<sup>30,31</sup>. A recent study has demonstrated optical-based  $O_2$  sensing in the deep peripheral tissue in living sheep using an ultrasound-powered optoelectronic device<sup>32</sup>; however, its deployment in the deep brain has not yet been accomplished.

Here we present a microscale, optoelectronic probe that wirelessly monitors in vivo  $p_{btO_2}$  signals in real time. The micro-probe measures local  $p_{btO_2}$  levels based on the quenching of phosphorescent dyes, whose optical signals are excited and collected via integrating a light-emitting diode (LED) and a photodetector. Miniaturized circuits, which can be powered using a battery or an inductive coil, capture and wirelessly transmit the  $p_{btO_2}$  data. In vitro and in vivo studies reveal the system's capability of dynamic  $p_{btO_2}$  recording, and the probe captures the cerebral hypoxia conditions with electrophysiological activities in a rodent seizure model.

## Results

### The microscale optoelectronic probe for $p_{btO_2}$ monitoring

We designed and fabricated a microscale optoelectronic probe to monitor  $p_{btO_2}$  changes in the deep brain (Fig. 1a,b). The detailed probe design and fabrication procedures are described in the Methods and Extended Data Fig. 1. From top to bottom (Fig. 1b), the micro-probe consists of a polydimethylsiloxane (PDMS) film embedded with platinum(II)-5,10,15,20-tetrakis-(2,3,4,5,6-pentafluorophenyl)-porphyrin (PtTFPP) phosphorescent dye, a PDMS/parylene encapsulation layer, an indium gallium nitride (InGaN) violet LED, a dielectric filter and an indium gallium phosphide (InGaP) photodetector on a copper-coated polyimide (PI) substrate. The sensing mechanism for  $p_{btO_2}$  operates on the principle of the photoluminescence (PL) quenching of PtTFPP with an increased level of  $p_{O_2}$  (ref. 33) (Fig. 1c,d). PtTFPP, at a concentration of 0.1 wt%, is mixed into the PDMS coating layer to obtain the optimal absorption and emission properties (Extended Data Fig. 2). The PtTFPP/PDMS film absorbs violet light (with an absorption peak at 389 nm) and shows a red PL emission peak at 646 nm (Fig. 1e). With an electroluminescence peak wavelength of 395 nm, the InGaP

violet LED serves as an excitation source for PtTFPP, whose PL emission is captured by the InGaP detector. Compared with previously reported implantable detectors based on silicon<sup>16</sup> or gallium arsenide (GaAs)<sup>34</sup>, the InGaP photodiode has a larger bandgap and therefore a smaller dark current density. In addition, InGaP is more stable than silicon and is less toxic than GaAs. The multilayered silicon dioxide/titanium dioxide-based longpass filter on the InGaP detector effectively optimizes its sensitivity in the red spectral range, resulting in a band-selective absorption between 570 and 655 nm. More details of these optical components are provided in the Methods, Extended Data Figs. 3 and 4 and Supplementary Tables 1 and 2. Collectively, the LED and the detector exhibit optical characteristics that are well-suited to the properties of PtTFPP (Fig. 1f). Figure 1g displays images of a fully integrated  $p_{btO_2}$ -sensing probe, and the PtTFPP/PDMS coating is approximately 30  $\mu\text{m}$  thick (Supplementary Fig. 1). On changing the environment from air to pure nitrogen ( $N_2$ ), the micro-probe exhibits a stronger red phosphorescence emission. Similar responses are observed when the micro-probe is inserted into a brain phantom, as shown in Fig. 1h.

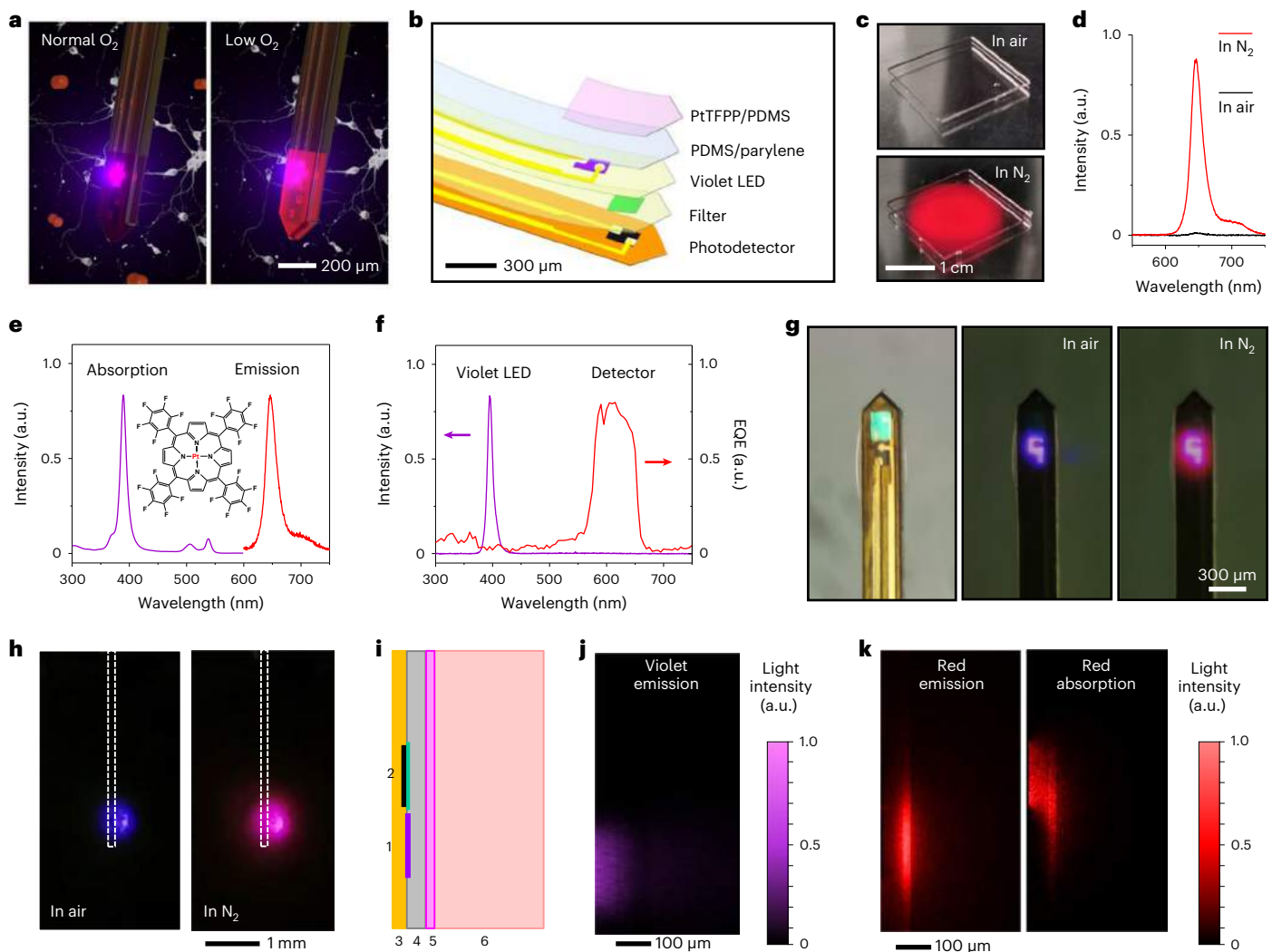
Furthermore, we established optical models to simulate the light distributions within the micro-probe and the surrounding tissue (Fig. 1i). Figure 1j demonstrates that the violet emission from the LED is predominantly absorbed by the PtTFPP/PDMS coating, with almost no leakage of PtTFPP into the surrounding tissue. By contrast, the down-converted red phosphorescence emitted by PtTFPP can penetrate more deeply into the tissue and be partially captured by the adjacent detector (Fig. 1k).

### In vitro performance of the $p_{btO_2}$ -sensing probe

We evaluated the performance of the micro-probe in a gas chamber with various  $O_2$  partial pressures ( $p_{O_2}$ ) by mixing  $N_2$  and  $O_2$  gas flows (Fig. 2a). At an LED injection current of 0.5 mA, the detector collects the PL intensity of the PtTFPP/PDMS coating at  $p_{O_2}$  levels from 0 to 70 mm Hg (Fig. 2b and Supplementary Fig. 2). The non-zero signals captured at high  $O_2$  pressure are mainly induced by the leaked violet light (Supplementary Fig. 3). The inverse of the PL intensity is linearly dependent on  $p_{O_2}$  and follows the Stern–Volmer equation (Fig. 2c)<sup>17</sup>. The nonlinear relationship between the PL intensity and  $p_{O_2}$  shows that the micro-probe is more sensitive to  $O_2$  fluctuations at lower  $p_{O_2}$  levels. At room temperature, the measured  $p_{O_2}$  detection resolutions are <0.8 mm Hg at  $p_{O_2} = 3.8$  mm Hg and <13 mm Hg at  $p_{O_2} = 56$  mm Hg (Supplementary Fig. 2). We also examined the dynamic response of the micro-probe to multiple cycles of alternated  $O_2$  and  $N_2$  flows (Fig. 2d). When the gas flow (10 litres per min) is switched between  $O_2$  and  $N_2$ , the recorded signal rise and decay times are 15.7 s and 0.9 s, respectively (Fig. 2e). The transient response of our micro-probe system is faster than previously reported techniques based on optical sensors and Clark electrodes<sup>23,31,32,35,36</sup>. In addition, the PL quenching mechanism in PtTFPP ensures that the micro-probe possesses high  $O_2$  selectivity over other gases, including  $N_2$  and  $CO_2$  (Fig. 2f). After the pretreatment, the micro-probe can continuously monitor  $p_{O_2}$  for over 2 h without any substantial photobleaching (Fig. 2g). Besides photostability, the micro-probe also exhibits desirable thermal stability (Fig. 2h). During in vitro and in vivo operation, the LED is driven by a pulsed current of 0.5 mA, which leads to a temperature rise of less than 1 °C (Supplementary Fig. 4). Therefore, the heating of the device has a minimal effect on the measurement accuracy and normal tissue function. Finally, the absorption of the PtTFPP/PDMS coating remains unchanged when immersed in phosphate-buffered saline (PBS) solution for over a month (Fig. 2i and Supplementary Fig. 5).

### Real-time, in vivo $p_{btO_2}$ monitoring with the wireless probe

For continuous  $p_{btO_2}$  monitoring in living animals, we applied the implantable optoelectronic probe with a customized wireless control circuit. As shown in Fig. 3a, the key components in the circuit involve



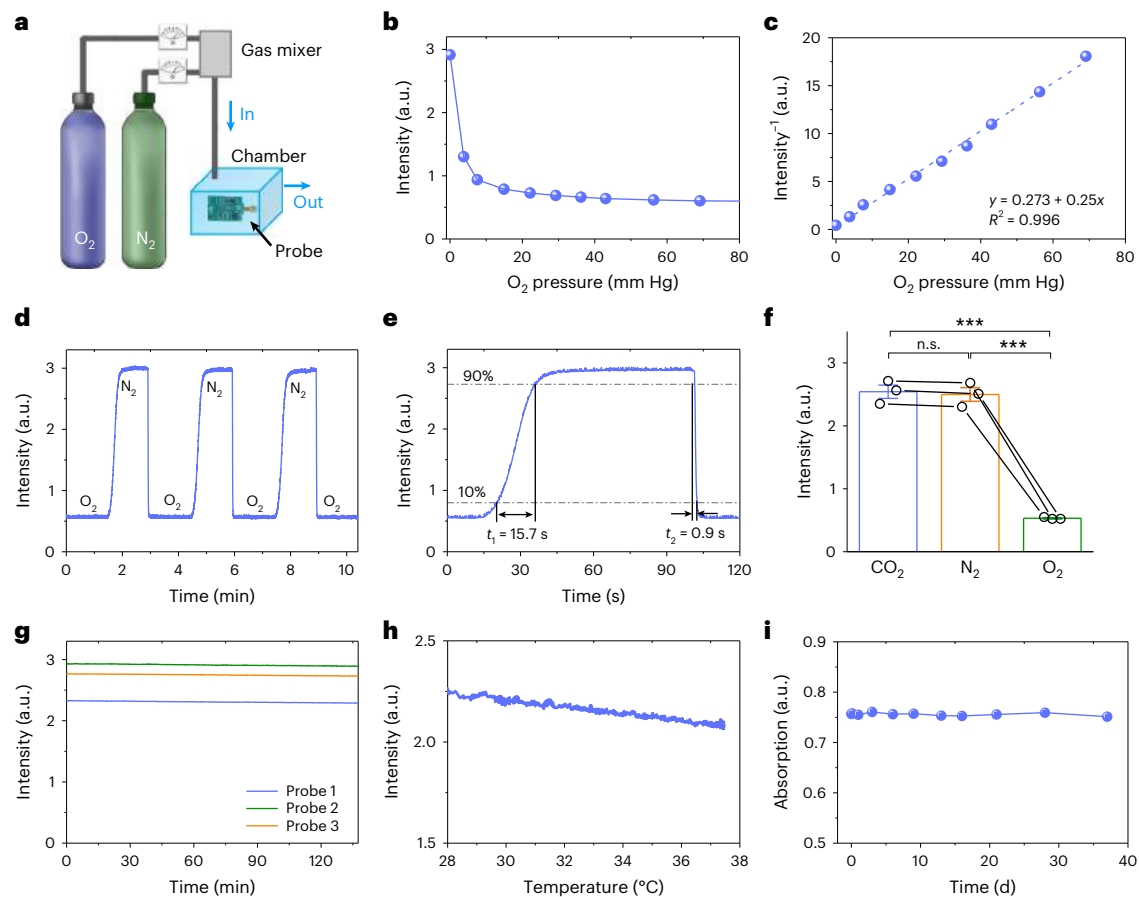
**Fig. 1 | Microscale optoelectronic probe for monitoring the oxygenation of brain tissue ( $p_{\text{btO}_2}$ ).** **a**, Schematic illustration of the probe implanted into brain tissue and optically responding to the change in  $\text{O}_2$  concentration (left: normal conditions; right: low  $\text{O}_2$  concentration). **b**, Enlarged view of the probe design, which includes (from top to bottom) a PtTFPP/PDMS sensing film, a PDMS/parylene encapsulation layer, an InGaN violet LED, a filter and an InGaP photodetector on a PI substrate. **c**, Photographs of a PtTFPP/PDMS film excited by violet light in air (top) and in a pure  $\text{N}_2$  environment (bottom). **d**, PL spectra of the PtTFPP/PDMS film in air and in  $\text{N}_2$ . **e**, Absorption and PL spectra of PtTFPP in PDMS. Inset: molecular structure of PtTFPP. **f**, Electroluminescence spectrum of

the violet LED and the external quantum efficiency (EQE) spectrum of the detector with a filter. **g**, Top-view optical images of a probe (left: LED is off; middle: LED is on in air; right: LED is on in  $\text{N}_2$ ). **h**, Experimental photographs comparing the light emission from a probe (side-view) implanted in a brain phantom in air (left) and in pure  $\text{N}_2$  (right). **i**, Schematic of the probe structure (side-view) used in the optical modelling: (1) LED; (2) detector with filter; (3) PI; (4) PDMS/parylene; (5) PtTFPP/PDMS; (6) brain tissue. **j**, Simulated intensity distribution of the violet excitation light from the LED. **k**, Simulated red PL emission from the PtTFPP dye (left) and that captured by the detector (right) in  $\text{N}_2$ .

an LED driver, an operational amplifier, a Bluetooth system on chip and a rechargeable battery. Data are converted to the corresponding  $p_{\text{btO}_2}$  values on the basis of in vitro calibrations for individual probes. The circuit module has a compact size of  $12.3 \times 17.3 \text{ mm}^2$  and a weight of 1.8 g (Fig. 3b, Supplementary Figs. 6 and 7 and Supplementary Table 3), and it is head-mounted on a freely moving mouse for the continuous monitoring of  $p_{\text{btO}_2}$  (Fig. 3c). To assess the sensing capability, we conducted acute tests on a mouse by dynamically varying the fraction of inspired  $\text{O}_2$  ( $F_{\text{iO}_2}$ ) using a mixture of inhaled  $\text{N}_2$  and  $\text{O}_2$  (Fig. 3d). The data collected by our wireless micro-probe agreed well with those collected simultaneously using a commercial fibre-optic sensor (NeoFox-GT, FOSPOR-AL300 probe, Ocean Insight) inserted into the same brain region (the bilateral hippocampus, at a depth of  $\sim 2.2 \text{ mm}$ ), suggesting that these systems exhibit a comparable performance (Fig. 3e). We also compared the in vivo performance of our wireless micro-probe with a carbon-based electrochemical electrode<sup>37</sup>, which

also yielded a similar temporal response (Extended Data Fig. 5). Furthermore, we used the micro-probe to record real-time  $p_{\text{btO}_2}$  data in mice during acute ischaemia/reperfusion cycles that were induced by clamping and declamping their bilateral carotid arteries (Fig. 3f). The recorded  $p_{\text{btO}_2}$  levels decreased to less than 3 mm Hg after clamping for about 1 min, and recovered after reperfusion (Fig. 3g). Another validation test monitored and compared the  $p_{\text{btO}_2}$  levels for mice in awake and anaesthetized states. The micro-probe recorded significantly higher  $p_{\text{btO}_2}$  levels in mice under isoflurane anaesthesia (Fig. 3h), consistent with previous studies<sup>38</sup>. Finally, and most importantly, the wireless circuit modules supported the acquisition and transportation of data from multiple micro-probes in multiple freely behaving animals, which is a feature scarcely achieved with the tethered fibre-optic system (Fig. 3i and Supplementary Video 1). When supplied with various  $F_{\text{iO}_2}$  values, the three animals exhibited similar fluctuations in  $p_{\text{btO}_2}$  (Fig. 3j). These explorations demonstrate the distinct advantages of





**Fig. 2 | In vitro characterization of the  $p_{btO_2}$ -sensing probe.** **a**, Illustration of the experimental setup for measuring the probe in response to different concentrations of  $O_2$ . The gas chamber has a size of  $10 \times 10 \times 6$  cm<sup>3</sup>, and the gas flows of  $N_2$  and  $O_2$  are varied. **b**, Recorded PL intensities at different  $O_2$  partial pressures. **c**, Calibration curve showing the linear relationship between the inverse of the PL intensity and the  $O_2$  partial pressure.  $R$ , coefficient of determination. **d**, Dynamic response of the probe at alternating  $O_2$  partial pressures (from 0 to 760 mm Hg). **e**, Partially enlarged curve of **d**, indicating a rise time  $t_1 = 15.7$  s and a decay time  $t_2 = 0.9$  s. **f**, Recorded signals of the probe

responding to different gases ( $CO_2$ ,  $N_2$  and  $O_2$ , at a pressure  $\sim 1$  atm or  $\sim 760$  mm Hg). One-way ANOVA (analysis of variance) and LSD (least significant difference) post-hoc comparison are performed ( $n = 3$  probes,  $***P < 0.001$ , n.s. (not significant)  $P > 0.05$ ). Values are presented as the mean  $\pm$  s.e.m. **g**, Signal stability of three different probes (LED injection current = 0.5 mA) measured at room temperature in pure  $N_2$ . **h**, Probe response at different temperatures (from 28 to 37.5 °C). **i**, Chronic stability of a PtTFPP/PDMS film. The film is immersed in PBS for more than one month and the peak absorption (at 390 nm) is measured on different days.

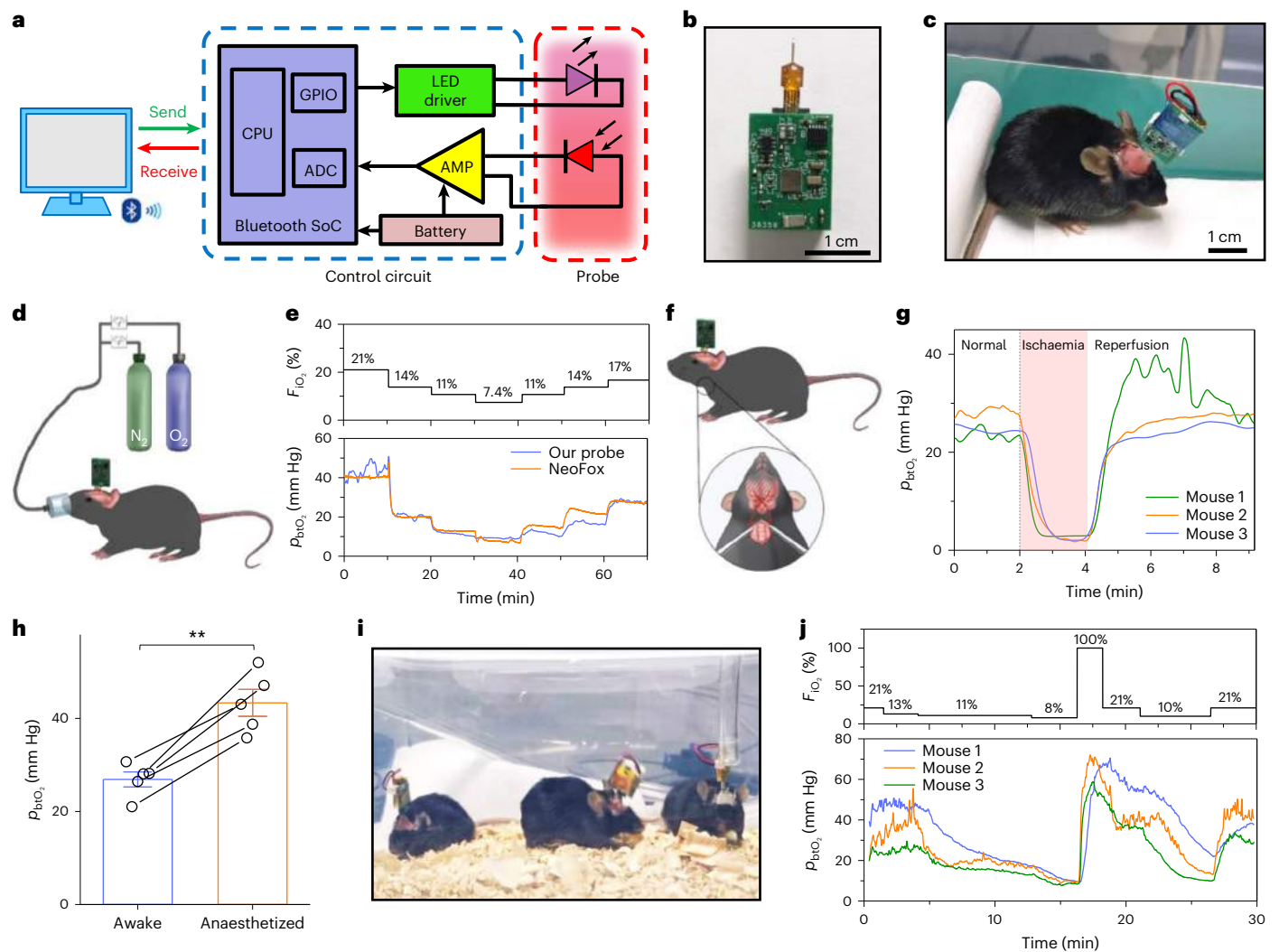
our wireless micro-probe in studying the real-time  $p_{btO_2}$  activities associated with complex animal behaviours and interactions.

### Dynamics of $p_{btO_2}$ under hippocampal electrical stimulation

In the mammalian brain, the  $p_{btO_2}$  level correlates strongly with local neural activity. Electrical stimulation of the hippocampus can lead to afterdischarges (ADs), and establishes the potential to trigger motor seizures<sup>39</sup>. Intense neural activity usually leads to an increase in local metabolism and  $O_2$  consumption, resulting in a decreased  $p_{btO_2}$  level. Utilizing our micro-probe, we investigated local variations in  $p_{btO_2}$  in response to electrical stimulation in the deep brain. As shown schematically in Fig. 4a, stimulating and recording electrodes were inserted into the hippocampus (CA1) of the mouse under study. Meanwhile, the optoelectronic micro-probe was implanted into the ipsilateral hippocampus (CA3) to continuously capture changes in  $p_{btO_2}$ . The surgical procedures are described in detail in Supplementary Fig. 8. Figure 4b and Supplementary Video 2 display the instance of a dramatic seizure event in a mouse, whose motion behaviours, local field potentials (LFPs) in CA1 and  $p_{btO_2}$  levels in CA3 are dynamically monitored simultaneously. In this example, 1-s-long pulsed kindling in CA1 elicits prominent ADs with intensified LFP oscillations and sometimes severe convulsion. The LFP bursts last for about 40 s, and then the micro-probe records a

dramatically decreased  $p_{btO_2}$  at the end of the animal convulsion, suggesting that intense neural activity causes increased local  $O_2$  consumption. The recorded time-invariant signals at a frequency of 50 Hz (Fig. 4b,e) are associated with the standard alternating current electricity. It is also noted that not every kindling can trigger an AD and associated  $p_{btO_2}$  drop, particularly when the time interval between the two stimuli is too short (Supplementary Fig. 9). Statistically, the CA3 region experiences severe hypoxia ( $p_{btO_2} < 10$  mm Hg) approximately 30 s after each AD, and recovers within about 60 s (Fig. 4c). This temporal relationship suggests that the local excessive neural activity leads to more  $O_2$  consumption by the neurons<sup>40</sup>, and the resulting hypoxia then suppresses neural activity and terminates the convulsive behaviour in mice<sup>41</sup>. To further understand the  $O_2$  evolution in the tissue, we established a diffusion model based on finite-element analysis (Extended Data Fig. 6). When both the  $O_2$  dissociation from  $HbO_2$  and the  $O_2$  transport are rapid<sup>42</sup>, abnormal conditions such as seizures can cause greatly intensified neural activity and excessive  $O_2$  consumption<sup>42</sup>, which cannot be fully compensated by the  $O_2$  supply and eventually leads to severe hypoxia.

Furthermore, we utilized the micro-probe to record the  $p_{btO_2}$  in a distant region (that is, the contralateral primary motor cortex (M1)) during hippocampal kindling in CA1 (Fig. 4d). As shown in Fig. 4e,f and Supplementary Video 3, the kindling-induced ADs can also elicit



**Fig. 3 | The probe combined with a wireless control circuit to continuously monitor  $p_{btO_2}$  in the brains of freely behaving mice.** **a**, Block diagram of the wireless system, comprised of a computer, a battery-powered control circuit and an implantable probe. **b**, Image of a probe connected with a wireless circuit. CPU, central processing unit; GPIO, general-purpose input/output port; ADC, analogue-to-digital converter; AMP, operational amplifier; SoC, system on chip. **c**, Photograph showing a freely behaving mouse with an implanted probe and the head-mounted circuit. **d**, Schematic of the setup showing that a wireless probe monitors the  $p_{btO_2}$  of a mouse provided with different fractions of inspired  $O_2$  ( $F_{IO_2}$ ). **e**, Dynamic change in  $F_{IO_2}$  (top) and  $p_{btO_2}$  results (bottom) detected

simultaneously by our wireless probe and a commercial fibre recording system (NeoFox, Ocean Optics). **f**, Schematic showing the probe to monitor the  $p_{btO_2}$  of a mouse during acute ischaemia/reperfusion induced by the clamping and declamping of its bilateral carotid arteries. **g**, Recorded  $p_{btO_2}$  results during acute ischaemia/reperfusion ( $n = 3$  mice). **h**, Comparison of  $p_{btO_2}$  results measured for mice in their awake and anaesthetized states. A paired  $t$ -test is performed ( $n = 5$  mice,  $**P < 0.01$ , the two-tailed  $P$  value is 0.002). Values are presented as the mean  $\pm$  s.e.m. **i**, Photograph of three freely moving mice with their  $p_{btO_2}$  values monitored simultaneously by wireless probes. **j**, Dynamic change in  $F_{IO_2}$  (top) and  $p_{btO_2}$  results (bottom) that are detected simultaneously in the three mice.

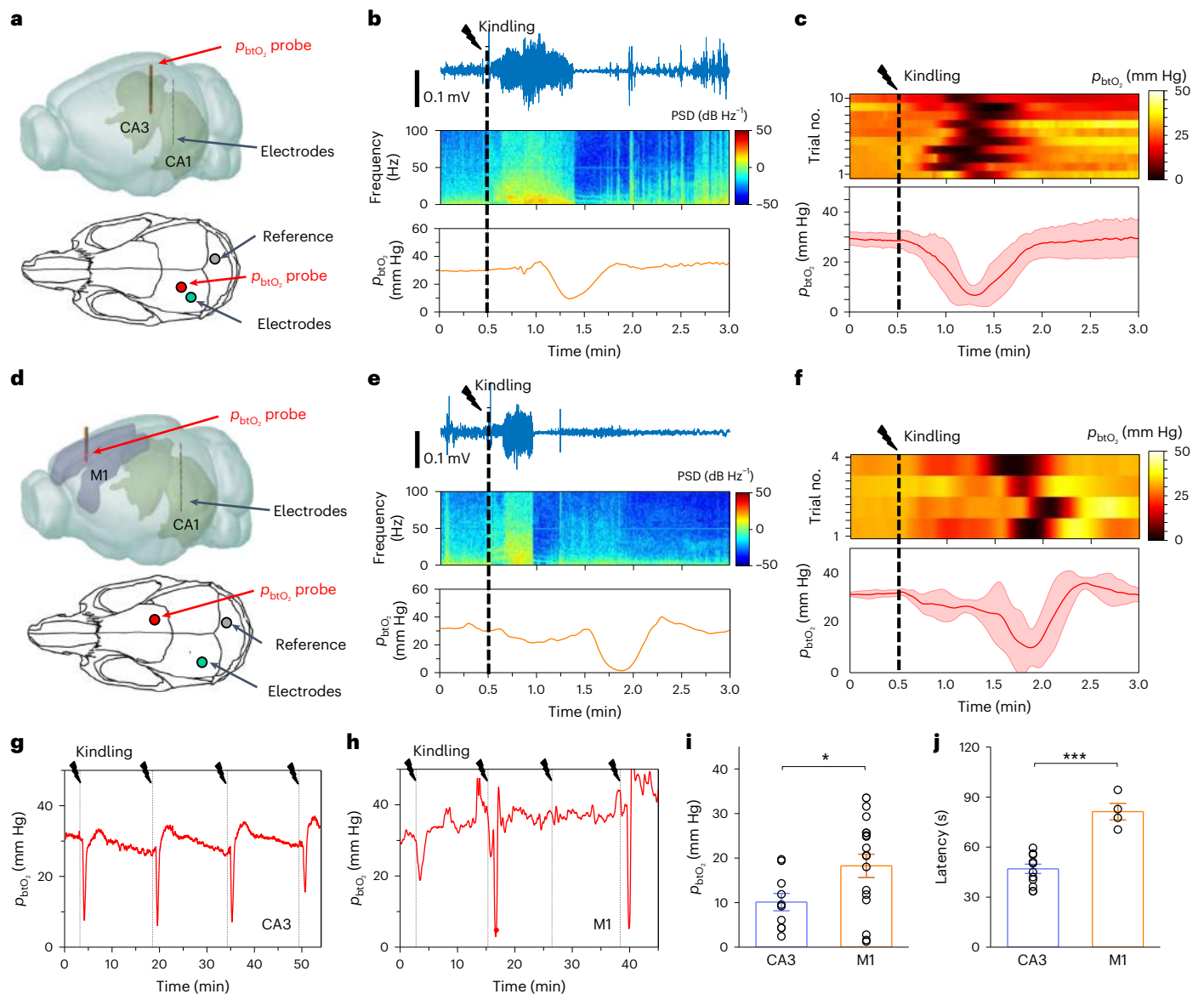
hypoxia in MI. Whereas almost every kindling in CA1 can induce a corresponding hypoxia event in the ipsilateral CA3 region (Fig. 4g), similar  $p_{btO_2}$  drops occur in approximately 25% of the trials (16 trials from four mice) (Fig. 4h). Compared with the results in CA3, similar hypoxia events observed in MI are less pronounced (Fig. 4i) and have a higher latency (Fig. 4j), which may be attributed to the migration of neural activity in the complex brain network<sup>43</sup>.

We further examines the blood  $O_2$  saturation in the same region (hippocampus) of the mice, based on the difference in optical absorption between  $HbO_2$  and  $Hb$  (Extended Data Fig. 7). Implanted into CA3, optical fibres measured the dynamic change in transmitted light at 660 and 810 nm, determining the  $S_{tO_2}$  in the cerebrovascular system (Extended Data Fig. 7a). When varying  $F_{IO_2}$ , the dynamic change in recorded  $S_{tO_2}$  is similar to that of  $p_{btO_2}$  (Extended Data Fig. 7b). Under kindling, however, the responses of these two signals are markedly different (Extended Data Fig. 7c). Whereas our  $p_{btO_2}$  probe captures

notable hypoxia, the optical fibre records the elevated  $S_{tO_2}$  immediately following the stimulation. Such a divergence clearly reveals that  $S_{tO_2}$  and  $p_{btO_2}$  are two distinct metabolic indicators.

### In vivo biocompatibility of the $p_{btO_2}$ -sensing probe

Histological analysis was used to characterize the biocompatibility of the  $p_{btO_2}$ -sensing probe in the hippocampal CA3 region of the mice. Through Nissl staining, the coronal section showed the lesion region created by the micro-probe (Supplementary Fig. 10). Results of immunofluorescence staining for glial fibrillary acidic protein (GFAP) at various stages of implantation reveal the astrocyte growth and the fibrosis formation surrounding the lesion region (Extended Data Fig. 8). Immunostaining of vascular endothelial cells (platelet endothelial cell adhesion molecule-1 (CD31)) and antibodies (immunoglobulin G (IgG)) enabled the tissue bleeding condition to be assessed at different stages after probe implantation (Extended Data Fig. 9).

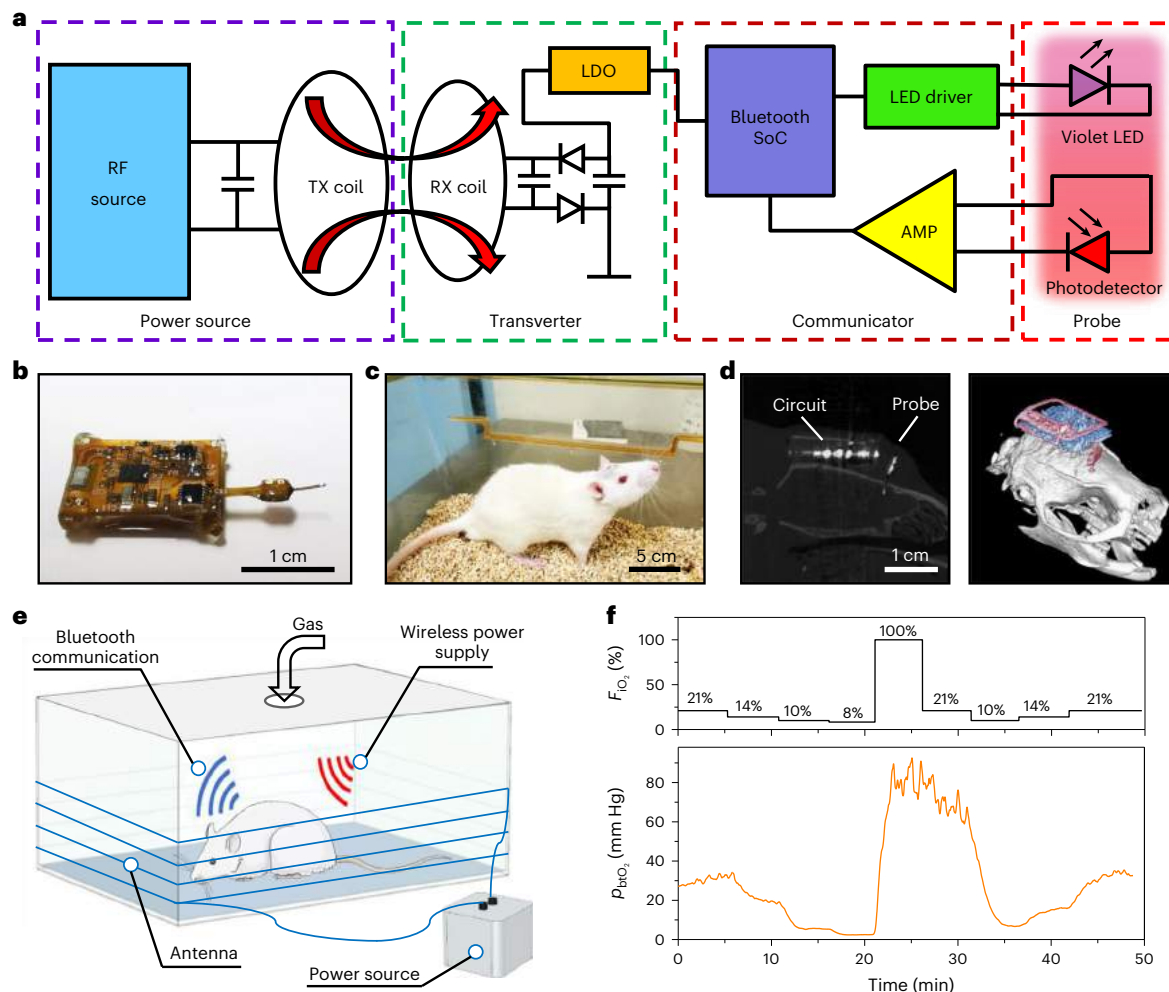


**Fig. 4 | Recording of  $p_{btO_2}$  signals in different brain regions of mice under electrical stimulation.** **a**, Three-dimensional (3D; upper) and two-dimensional (2D; lower) schematics showing the positions of the  $p_{btO_2}$  sensing probe (CA3) and the stimulating/recording electrodes (CA1) implanted in the ipsilateral hippocampus of mice. **b**, Simultaneously recorded electrophysiological activities in CA1 and  $p_{btO_2}$  in CA3 under kindling: LFP trace (top); power spectral density (PSD) of the LFP (middle);  $p_{btO_2}$  profile (bottom). **c**, Dynamic response of  $p_{btO_2}$  recorded in CA3: heatmap of ten individual trials from  $n = 10$  mice (top); average  $p_{btO_2}$  signals (bottom). The solid lines and shaded areas indicate the mean and s.e.m., respectively. **d**, 3D (upper) and 2D (lower) schematics showing the positions of the  $p_{btO_2}$  probe and the electrodes implanted in the contralateral primary motor cortex (M1) and the hippocampus (CA1) of mice. **e**, Simultaneously recorded electrophysiological activities in CA1 and  $p_{btO_2}$  in M1

under kindling: LFP trace (top); PSD of the LFP (middle);  $p_{btO_2}$  profile (bottom). **f**, Dynamic response of  $p_{btO_2}$  recorded in M1: heatmap of four individual trials from  $n = 3$  mice (top); average  $p_{btO_2}$  signals (bottom). The solid lines and shaded areas indicate the mean and s.e.m., respectively. **g, h**, Continuously monitored  $p_{btO_2}$  in CA3 (**g**) and M1 (**h**) during sequential kindlings for multiple times. **i**, Comparison of the lowest  $p_{btO_2}$  values recorded in the ipsilateral CA3 (ten trials,  $n = 5$  mice) and contralateral M1 (16 trials,  $n = 4$  mice) regions after kindling in CA1. ( $*P < 0.05$ , the two-tailed  $P$  value is 0.036.) **j**, Comparison of the latency time from kindling in CA1 to reaching the lowest  $p_{btO_2}$  in CA3 (ten trials,  $n = 5$  mice) and M1 (four trials,  $n = 3$  mice). ( $***P < 0.001$ , the two-tailed  $P$  value is 0.000038.) For **i** and **j**, the statistical analysis is based on the  $t$ -test of independent samples. Values are presented as mean  $\pm$  s.e.m.

Moreover, we assessed the chronic operation properties of the micro-probe in vivo (Supplementary Fig. 11). Device degradation and failure occurred after nine days, which was due mainly to water penetration into the tissue. Multilayered inorganic/organic encapsulants will enhance the water resistance of the devices<sup>44</sup>. Further optimizations could involve a reduction of the probe size and surface modifications with more biocompatible coatings, such as hydrogels<sup>45</sup>, to minimize tissue damage, alleviate fibrosis and mitigate bleeding.

**A fully implanted, battery-free probe for  $p_{btO_2}$  monitoring**  
A further technical advance involved the development of a wireless, battery-free circuit module that can be fully implanted subcutaneously, as detailed in Fig. 5a and Supplementary Figs. 12 and 13. Compared with the battery-powered probe, such a battery-free system possesses improved flexibility, reduced weight and longer-lasting data collection without interruption. Protected by a waterproof encapsulant, the entire circuit can be fully implanted under the scalp of freely behaving rats (Fig. 5b,c and Supplementary Fig. 14). X-ray computed tomography



**Fig. 5 | A fully implanted, battery-free probe system monitors  $p_{btO_2}$  in the brain of living rats. a**, Block diagram of the system, which includes an RF power source, a receiving coil, a Bluetooth communication module and an implantable probe. TX, primary coil (transmitted power); RX, secondary coil (received power); LDO, low-dropout regulator. **b**, Image of the probe connected with the battery-free circuit. **c**, Photograph showing a freely moving rat with a fully

implanted probe system. **d**, Sagittal CT image indicating the location of the implanted system in a rat (left), and reconstructed 3D CT image showing the position of the device relative to the skull (right). **e**, Schematic illustration of the setup for monitoring  $p_{btO_2}$  in rats. **f**, Results of the dynamic change in  $F_{iO_2}$  (top) and  $p_{btO_2}$  (bottom) monitored in a rat.

(CT) images revealed the location of the  $p_{btO_2}$  probe in the rat brain as well as the position of the circuit module (Fig. 5d). As the power transverter, a looped antenna receives currents from an external radio-frequency (RF) source and generates magnetic fields in an enclosure to study the behaviour of the animals (Fig. 5e and Supplementary Fig. 15). Under normal operation, the circuit experienced a temperature rise of less than 3.5 °C, ensuring its safety within the body of the animal (Supplementary Fig. 16). The proof-of-concept study presented in Fig. 5f demonstrates the wireless and continuous monitoring of  $p_{btO_2}$  in a rat in response to changes in  $F_{iO_2}$  over a period of around 50 min.

## Discussion

Supplementary Table 4 compares the characteristics of our micro-probe with those of previous reports. Different from probe systems that sense blood oxygenation (Hb and HbO<sub>2</sub>)<sup>15,46</sup>, our micro-probe explores cerebral oxygenation through  $p_{btO_2}$ . The utilization of a microscale device and a thin-film PtTFPP/PDMS coating guarantees a small tissue lesion and a prompt response (<1 s).

In this study, we monitored the changes in  $p_{btO_2}$  induced by electrical stimuli in a seizure model. As a future endeavour, it will be more beneficial to investigate  $p_{btO_2}$  before, during and after the occurrence of spontaneous seizures. Although PtTFPP is capable of capturing

hypoxic events ( $p_{btO_2} < 20$  mm Hg), its insensitivity at higher O<sub>2</sub> pressures (>20 mm Hg) limits its application in detecting both normal and hyperoxic conditions. In the future, alternative luminophores<sup>47</sup> could be exploited to extend the sensing window to elevated O<sub>2</sub> levels. Our current micro-probe monitors  $p_{btO_2}$  in a relatively large brain region (~200 μm) in the hippocampus of mice during ADs that last for tens of seconds. Prospectively, a probe with a much reduced footprint and a faster response would be highly desirable for the detection of more rapid O<sub>2</sub> dynamics in a smaller region or even at the cellular scale.

Besides recording the PL intensity, advanced circuit systems could enable the detection of  $p_{btO_2}$  based on PL lifetime changes, which are less susceptible to dye photobleaching and have the potential to provide more accurate measurements<sup>27</sup>. Meanwhile, the combination of electrophysiological activities,  $p_{btO_2}$  and blood oxygenation will foster a more profound understanding of neurovascular and neurometabolic coupling. Both battery-powered and battery-free circuit schemes have been introduced for the monitoring of  $p_{btO_2}$  in the rodent brain, and they can also be feasible for clinical applications. The two strategies can be combined to realize a stable power supply and wireless charging simultaneously<sup>48,49</sup>. The presented technique clearly indicates its potential utility in neuroscience research and medical diagnostics.



## Online content

Any methods, additional references, Nature Portfolio reporting summaries, source data, extended data, supplementary information, acknowledgements, peer review information; details of author contributions and competing interests; and statements of data and code availability are available at <https://doi.org/10.1038/s41566-023-01374-y>.

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## Methods

### Device fabrication

Details on the device structures and fabrication processes are provided in the Supplementary Information, Supplementary Figs. 1–4 and Supplementary Tables 1 and 2. The InGaP photodetector structure is grown on a GaAs substrate, and the InGaN violet LED structure is grown on sapphire, both via metal–organic chemical vapour deposition. Both the detector and the LED were fabricated using a standard photolithographic process, and freestanding, thin-film microscale devices were formed by selectively etching the  $\text{Al}_{0.95}\text{Ga}_{0.05}\text{As}$  sacrificial layer (for the detector)<sup>34</sup> or via ultraviolet laser liftoff (for the LED)<sup>50</sup>. The multilayered silicon dioxide/titanium dioxide longpass filter was deposited onto the GaAs substrate via ion beam-assisted sputtering, with freestanding, thin-film filters formed through femtosecond laser milling and wet etching<sup>51</sup>. A detector, an optical filter and a violet LED were sequentially transferred onto the flexible substrate with PDMS stamps<sup>52</sup>, followed by insulation with SU-8 photoresist and metalization. Laser milling (355 nm ultraviolet laser, LPKF ProtoLaser U4) was used to define the needle shape (width  $\sim 300\ \mu\text{m}$ , length  $\sim 3\ \text{mm}$ ). Sputtered Cr/Au/Cu/Au layers (6 nm/100 nm/600 nm/150 nm, respectively) served as the interconnect contacts for the devices. Laser milling was used to form the shape of the micro-probes. After encapsulation by PDMS and parylene C, the  $\text{O}_2$ -sensing film (PtTFPP/PDMS) was dip-coated onto the tip of the probe.

### Device characterization and modelling

**Characterization of the  $p_{\text{btO}_2}$ -sensing probe.** In vitro characterization of the  $p_{\text{btO}_2}$ -monitoring probe was carried out using a gas chamber of size  $10 \times 10 \times 6\ \text{cm}^3$ , with the gas flow from a gas mixer with two gas flowmeters connected to supplies of pure  $\text{N}_2$  (range:  $\sim 0$ –25 litres per min, resolution: 2.5 litres per min) and pure  $\text{O}_2$  (range:  $\sim 0$ –1 litres per min, resolution: 0.05 litres per min). The  $p_{\text{O}_2}$  level was controlled using the two gas flowmeters. Before calibration, the probe underwent photobleaching pretreatment in a pure  $\text{N}_2$  environment by supplying the LED with a constant current of 0.5 mA for 30 min. During the in vitro testing, the probe was operated with a sampling frequency of 4 Hz and a driver current of 0.5 mA at a pulse width of 10 ms. The thermal stability testing was performed in a PBS solution containing  $\text{Na}_2\text{SO}_3$  (5% w/v).

**Optoelectronic characterization.** The emission spectra of the  $\text{O}_2$ -sensitive film and the LED were measured with a high-resolution spectrometer (HR 2000+, Ocean Optics). The absorption spectra of the  $\text{O}_2$ -sensitive film and the transmission spectra of the filter and the PI film were measured using a spectrophotometer (Cary 5000, Agilent Technologies). The current–voltage characteristics of the LED and photodetector were recorded using a Keithley 2400 source meter. The EQE values of the LED and the detector were determined using a spectroradiometer with an integrating sphere (Labsphere). For the in vitro tests, the micro-probes were implanted into a brain phantom made of agarose (0.5% w/v), Hb (0.2% w/v) and a lipid emulsion (Intralipid; 1% w/v) mixed in PBS (98.3% w/v). After stirring, the mixed liquid was heated to boiling, then cooled to room temperature to form a gel.

**Optical modelling.** A ray-tracing method based on Monte Carlo simulations (TracePro free trial version) was used to simulate the light distribution in the brain. In this model, an LED with a size of  $190 \times 110 \times 10\ \mu\text{m}^3$  emits light at a wavelength of 395 nm, and a detector ( $185 \times 125 \times 3\ \mu\text{m}^3$ ) was placed adjacent to the LED. The LED emission has a Lambertian distribution and was modelled with 1,000,000 rays. A polymer layer with a thickness of  $50\ \mu\text{m}$  and a layer of  $\text{O}_2$ -sensitive film with a thickness of  $25\ \mu\text{m}$  were coated onto both devices. The refractive index values of the polymer layer and the  $\text{O}_2$ -sensitive film are 1.44 at 395 nm and 1.41 at 650 nm, respectively. The  $\text{O}_2$ -sensitive film has a phosphorescence conversion efficiency of 0.19, a peak molar extinction of  $300,000\ \text{M}^{-1}\ \text{cm}^{-1}$  and a molar concentration of 0.85 mM. The probe was inserted into

the brain tissue (size  $5 \times 5 \times 5\ \text{mm}^3$ ) with absorption coefficients of  $0.75\ \text{mm}^{-1}$  and  $0.08\ \text{mm}^{-1}$ , and scattering coefficients of  $30\ \text{mm}^{-1}$  and  $33\ \text{mm}^{-1}$ , for violet (395 nm) and red (650 nm) light, respectively. The tissue had an anisotropy factor of 0.85 and a refractive index of 1.36.

**Thermal measurements and modelling.** The temperature distributions on the surface of the probe and the circuit board were mapped using an infrared camera (FOTRIC 228). The emissivity values of the probe surface, the surface of the battery-free circuit and the surface of the battery-powered circuit were set to 0.95, 0.95 and 0.80, respectively. A 3D steady-state heat-transfer model was established using finite-element analysis (COMSOL Multiphysics). The materials and the respective corresponding parameters (density, thermal conductivity and heat capacity) used in the model are as follows: parylene ( $1.11\ \text{g cm}^{-3}$ ,  $0.086\ \text{W m}^{-1}\ \text{K}^{-1}$ ,  $3.5\ \text{J g}^{-1}\ \text{K}^{-1}$ ), PDMS ( $0.965\ \text{g cm}^{-3}$ ,  $0.15\ \text{W m}^{-1}\ \text{K}^{-1}$ ,  $1.46\ \text{J g}^{-1}\ \text{K}^{-1}$ ), PI ( $1.4\ \text{g cm}^{-3}$ ,  $0.15\ \text{W m}^{-1}\ \text{K}^{-1}$ ,  $1.1\ \text{J g}^{-1}\ \text{K}^{-1}$ ), Cu ( $8.96\ \text{g cm}^{-3}$ ,  $400\ \text{W m}^{-1}\ \text{K}^{-1}$ ,  $0.385\ \text{J g}^{-1}\ \text{K}^{-1}$ ), SU-8 ( $1.2\ \text{g cm}^{-3}$ ,  $0.2\ \text{W m}^{-1}\ \text{K}^{-1}$ ,  $1.5\ \text{J g}^{-1}\ \text{K}^{-1}$ ). The boundary condition was natural heat convection to air at  $25\ ^\circ\text{C}$ . The LED served as the heat source, with the input thermal power estimated via  $P = V \times I \times (1 - \text{EQE})$ , where  $V$ ,  $I$  and EQE are the measured voltage, current and corresponding EQE values for the LEDs. The measured and simulated thermal distribution of the probe surface is shown in Supplementary Fig. 4.

**Modelling of  $\text{O}_2$  transport.** A 2D diffusion model based on the finite-element analysis method (COMSOL Multiphysics) was used to calculate the spatial distribution and the temporal change in  $p_{\text{O}_2}$  in the brain tissue (Extended Data Fig. 6). The tissue region was of a circular shape with a diameter of  $500\ \mu\text{m}$ , in which there were arrays of capillaries with a diameter of  $10\ \mu\text{m}$  and a spacing of  $50\ \mu\text{m}$  (Extended Data Fig. 6a). The values of  $p_{\text{O}_2}$  in the capillaries and the tissue outer boundary were fixed to 50 mm Hg and 30 mm Hg, respectively. The dissociation of  $\text{O}_2$  from  $\text{HbO}_2$  is very rapid and is considered to be instantaneous<sup>42</sup>. Embedded into the tissue, the implantable probe (length  $200\ \mu\text{m}$ ) comprised a PtTFPP/PDMS-based  $\text{O}_2$ -sensitive film (thickness  $30\ \mu\text{m}$ ) and a gas-impermeable substrate (thickness  $30\ \mu\text{m}$ ). The diffusivities of  $\text{O}_2$  in the brain tissue and the PtTFPP/PDMS film are  $1.6 \times 10^{-5}\ \text{cm}^2\ \text{s}^{-1}$  and  $4 \times 10^{-5}\ \text{cm}^2\ \text{s}^{-1}$ , respectively<sup>53,54</sup>. The relationship between  $p_{\text{O}_2}$  and the molar concentration of dissolved  $\text{O}_2$  ( $c_{\text{O}_2}$ ) follows Henry's law:  $c_{\text{O}_2} = p_{\text{O}_2} \times \alpha / V_m$ , where  $\alpha = 0.022\ \text{ml ml}^{-1}\ \text{atm}^{-1}$  is the  $\text{O}_2$  solubility in tissue<sup>53</sup> and  $V_m = 25.4$  litres per mol is the gas molar volume at  $37\ ^\circ\text{C}$  and 1 atm. During the resting state, the oxygen consumption rate (OCR) was set to  $33\ \mu\text{mol litre}^{-1}\ \text{s}^{-1}$  (ref. 55). Enhanced neural activity after kindling is assumed to increase the OCR, with a Gaussian function having a peak six times that of the resting state<sup>12</sup> (Extended Data Fig. 6b, top).

### Wireless circuit design

A customized circuit module was designed to operate the LED wirelessly and receive signals from the detector, and a computer or a mobile phone controlled the monitoring system and received the  $p_{\text{btO}_2}$  signals. The schematic diagram and layout of the printed circuit board for the battery-powered circuit design are depicted in Supplementary Figs. 6 and 7, respectively. A programmable microcontroller (nRF52832, Nordic Semiconductor) was operated at 2.4 GHz for wireless data communication. An LED driver (LTC3212, Analog Devices) with an external resistor supplied a stable current to the LED. The photocurrent of the detector was amplified using an operational amplifier (OPA391, Texas Instruments), and was then digitized by the microcontroller's analogue-to-digital converter for wireless transmission. A linear regulator (NCP161, ON Semiconductor) with a fixed internal output voltage (3.3 V) ensured a stable power supply. The battery-powered circuit had a size of  $17.3 \times 12.3\ \text{mm}^2$  and a weight of 1.8 g (which included a rechargeable lithium-ion battery with a weight of 1.2 g). The battery had a capacity of 45 mAh and could work continuously for more than eight hours.

The circuit was connected to the implanted probe via a flexible connector. When animals are freely moving, the motion artefact is a major source of noise. The collected raw data were processed via LOWESS (locally weighted scatterplot smoothing) to reduce the high-frequency, zero-mean noise caused by the motion of the animals.

The design of the battery-free circuit was similar to that of the battery-powered circuit, except that it was powered through inductive coupling. The schematic diagram and layout of the fully implanted battery-free circuit are displayed in Supplementary Figs. 12 and 13, respectively. The flexible printed circuit board is based on PI/Cu foils, and an inductive coil with seven turns was used for the power supply. Two capacitors in parallel ( $\sim 62$  pF) were used to tune the power-harvesting antenna. The half-bridge rectifier was made up of two Schottky diodes (Skyworks) and a capacitor (2.2  $\mu$ F). Located in a cage enclosed by a copper wire antenna with four loops, the  $p_{\text{btO}_2}$  of the freely behaving rats can be monitored continuously using the fully implanted micro-probe. Electromagnetic finite-element analysis was applied to simulate the magnetic field distribution inside an enclosure measuring  $23.0 \times 16.0 \times 6.5$  cm<sup>3</sup> (Supplementary Fig. 15). The antenna was operated at 13.56 MHz, and the output power was 4 W. The maximum temperature rise of the wireless circuit tested at room temperature was less than 3.5 °C (Supplementary Fig. 16).

### Biological studies

**Animals.** All animal procedures were approved by the Institutional Animal Care and Use Committee at Tsinghua University. Adult (8–12-week-old) male wild-type C57BL/6N mice and adult male Sprague–Dawley rats (body weight 350–550 g) purchased from the Vital River Laboratory (Animal Technology) were used and housed in groups (3–5 mice per cage, 1–2 rats per cage) under standard conditions. The animals were maintained on a 12 h light/dark cycle at 22–25 °C and had access to food and water ad libitum.

**Stereotaxic surgery.** The adult wild-type mice were anaesthetized via an intraperitoneal injection of Avertin (280 mg per kg (body weight)) before surgery and then placed in a standard stereotaxic instrument for surgical implantation. After shaving the scalp and exposing the skull, small holes of  $\sim 0.5$  mm diameter were drilled in the skull using a micromotor drill. For mice that received electrical stimulation, the  $p_{\text{btO}_2}$ -sensing probes were implanted slowly in the hippocampus at CA3 (anterior–posterior (AP):  $-1.8$  mm, medial–lateral (ML):  $\pm 1.86$  mm, dorsal–ventral (DV):  $-2.25$  mm) or M1 (AP:  $1.15$  mm, ML:  $1.7$  mm, DV:  $-2$  mm), and a small amount of dental cement was used to fix the probe. For  $S_{\text{tO}_2}$  sensing, two optical fibres were individually implanted in the hippocampus at an incline (AP:  $-1.8$  mm, ML:  $0.7$  mm, DV:  $-1.9$  mm, angle:  $23^\circ$ ; and AP:  $-1.8$  mm, ML:  $2.5$  mm, DV:  $-1.9$  mm, angle:  $12^\circ$ ). The stimulating/recording electrodes were constructed of twisted Teflon-coated tungsten wires (catalogue no. 796000, A-M Systems) and targeted to the hippocampal CA1 region (AP:  $-3.0$  mm, ML:  $-2.9$  mm, DV:  $-3.2$  mm). A stainless steel screw acted as the reference electrode and was implanted in the skull. Finally, more dental cement was used to fix all devices on the skull (Supplementary Fig. 8).

The battery-free circuit was fully implanted in the Sprague–Dawley rats after they had been anaesthetized via an intraperitoneal injection of mixed Zoletil and xylazine (8 and 15 mg per kg (body weight), respectively). After being placed in a standard stereotaxic instrument for surgical implantation, an incision in the scalp was made to expose the skull. Then, 0.3% hydrogen peroxide was applied to clean the skull, and a small hole with a diameter of  $\sim 0.5$  mm was drilled. The probe was implanted into the brain (AP:  $3.6$  mm, ML:  $2.0$  mm, DV:  $-2.9$  mm), and dental cement was applied to fix the device to the skull followed by suturing of the scalp (Supplementary Fig. 14). To allow the animals to recover, in vivo measurements on the mice and rats were conducted at least four days after surgery.

**In vivo  $p_{\text{btO}_2}$  monitoring.** Clamping and declamping of the bilateral carotid arteries was performed on the mice anaesthetized with Avertin (280 mg per kg (body weight)). Under anaesthesia, the wireless circuit was connected to the probe fixed on the mouse skull; the mouse was then placed in a supine position and a small incision was made in the middle of the anterior neck. Next, the muscles under the skin were removed and the bilateral common carotid artery (CCA) was exposed. The left CCA was ligated using a small artery clip, and then the right CCA was ligated. After monitoring for about 2 min, the clips were removed to restore the blood flow.

The micro-probes were used to monitor the  $p_{\text{btO}_2}$  of freely behaving mice under various  $F_{\text{IO}_2}$  conditions. One or multiple mice were placed in a gas chamber (size  $16.0 \times 23.0 \times 13.5$  cm<sup>3</sup>), and the inflowing gas was controlled via two flowmeters connected to pure N<sub>2</sub> and pure O<sub>2</sub>. The ratio of the N<sub>2</sub> and O<sub>2</sub> flow rates was varied to achieve different  $p_{\text{O}_2}$  values.

The  $p_{\text{btO}_2}$  of the awake mice was measured 5 min after they had been placed the gas chamber with an airflow of 2 litres per min, and their  $p_{\text{btO}_2}$  in an anaesthetized state was measured after 5 min in flowing air mixed with 2% isoflurane.

Electrical stimulation/kindling was applied to the hippocampal CA1 region of the mice at least four days after surgery. This protocol involved a biphasic pulse train with a current of 0.4 mA, a pulse frequency of 60 Hz and a pulse width of 1 ms, administered for a duration of 1 s. Sequential kindling was applied with a time interval of no less than 10 min for eight times each day until a seizure occurred (usually  $\sim 2$ –4 days after kindling). LFP recording and electrical stimulation were accomplished using an electrophysiological recording system (alphaRS Pro, Alpha Omega Engineering), and the implanted micro-probe simultaneously recorded the  $p_{\text{btO}_2}$  signals wirelessly.

**In vivo  $S_{\text{tO}_2}$  monitoring.** The dynamic  $S_{\text{tO}_2}$  signals in the hippocampus regions of mice were recorded using a fibre-based setup. A stimulating electrode was implanted in the hippocampal CA1 region, while two fibres (diameter 0.2 mm) were located around the ipsilateral CA3 region. One fibre was coupled to the two LED sources (M660FP1, M810F2, Thorlabs) that emitted alternating red (660 nm) and infrared (810 nm) light (frequency 100 Hz), and the other fibre was coupled to a photodetector (LSSPD-2.5, Beijing Lightsensing Technologies) to receive the signal. The distance between the two fibre ends was about 0.5 mm. The cerebral  $S_{\text{tO}_2}$ , which is the percentage of HbO<sub>2</sub> (ranging from 0 to 100%), was calculated based on the modified Beer–Lambert law<sup>56</sup>. The normal  $S_{\text{tO}_2}$  level (baseline) was set to 85%, and the total Hb concentration was set to 2.3 mM. The optical properties of brain tissue and blood were obtained from the literature<sup>57</sup>.

**Immunofluorescence staining.** The mouse brains were fixed with 4% paraformaldehyde (PFA) in PBS and subjected to gradient dehydration, embedded in optimal cutting temperature compound (SAKURA 4583), frozen and sectioned into 10- $\mu$ m-thick slices using a freezing microtome (Leica 3050S). The sections were incubated with PBS containing 2% bovine serum albumin and 0.5% Triton-X-100 for one hour at room temperature, followed by incubation overnight at 4 °C in PBS containing 2% bovine serum albumin and 0.5% Triton-X-100 with appropriate dilutions of the following primary antibodies: anti-GFAP (ab7260, Abcam; 1:400) and anti-CD31 (AF4709, R&D Systems; 1:40). Then, the sections were washed three times (for 5 min each) at room temperature in PBS, followed by incubation with secondary antibodies (Alexa Fluor 488 donkey anti-goat IgG antibodies: A-11055, 1:1,000; Alexa Fluor 647 donkey anti-rabbit IgG antibodies: A-31573, 1:1,000; Alexa Fluor 555 donkey anti-chicken IgG antibodies: A78949, 1:1,000, all from Thermo Fisher Scientific) for one hour at room temperature. After 5 min in 1:10,000 DAPI (4',6-diamidino-2-phenylindole) reagent, the sections were washed with PBS again and mounted with coverslips. Images were acquired using a fluorescence microscope (Mica, Leica).



**Nissl staining.** Mice were anaesthetized with Avertin (280 mg per kg (body weight)) and perfused intracardially with PBS and PFA. The brains were post-fixed in PFA overnight. Coronal brain paraffin sections were taken with a thickness of 5  $\mu\text{m}$  and then deparaffinized with xylene twice (for 20 min each). These sections were rinsed with anhydrous alcohol twice (for 5 min each) and 75% alcohol for 5 min. Then, they were rinsed with tap water and distilled water. After immersion in 0.03% toluidine blue solution (pH = 1.5) for 2–5 min, the samples were washed with tap water. The sections were cleared in xylene for 10 min and mounted using permanent mounting media.

## Data availability

The data that support the plots within this paper are available in the Supplementary Information. Source data are provided with this paper.

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## Author contributions

X.C., D.S., Z.L., B.Z., G.T., W.Z., Y.X. and X.F. performed the device design, fabrication and characterization. X.C., H.Z., Z.Y., Z.X. and H.D. designed and tested the circuits. X.C., P.W., Q.L., D.S., Y.D., C.W. and Y.W. designed and performed the biological experiments. P.W., C.W., L.Y., H.P., H.D., G.Z. and X.S. provided the tools and supervised the research. X.C., H.D. and X.S. wrote the paper in consultation with the other authors.

## Competing interests

The authors declare no competing interests.

## Additional information

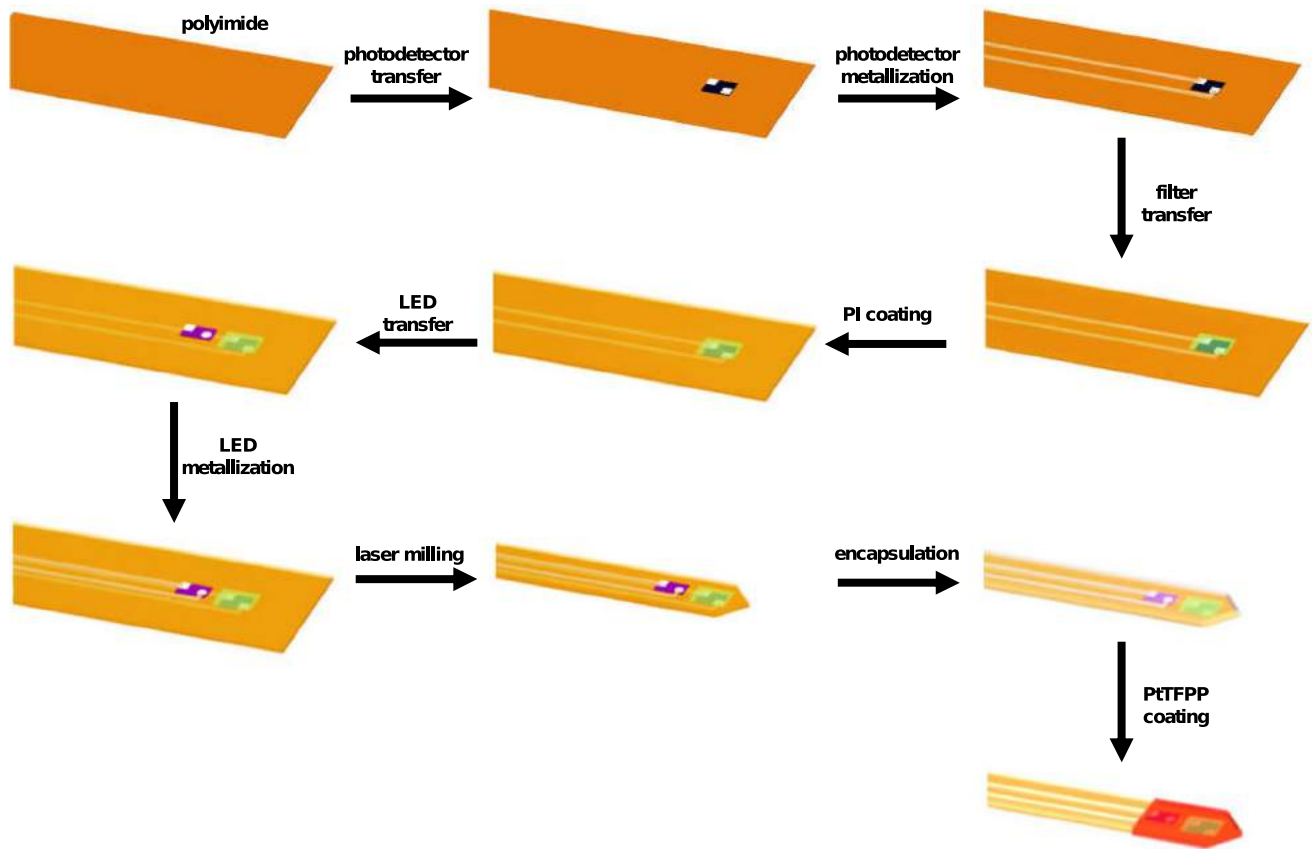
**Extended data** is available for this paper at <https://doi.org/10.1038/s41566-023-01374-y>.

**Supplementary information** The online version contains supplementary material available at <https://doi.org/10.1038/s41566-023-01374-y>.

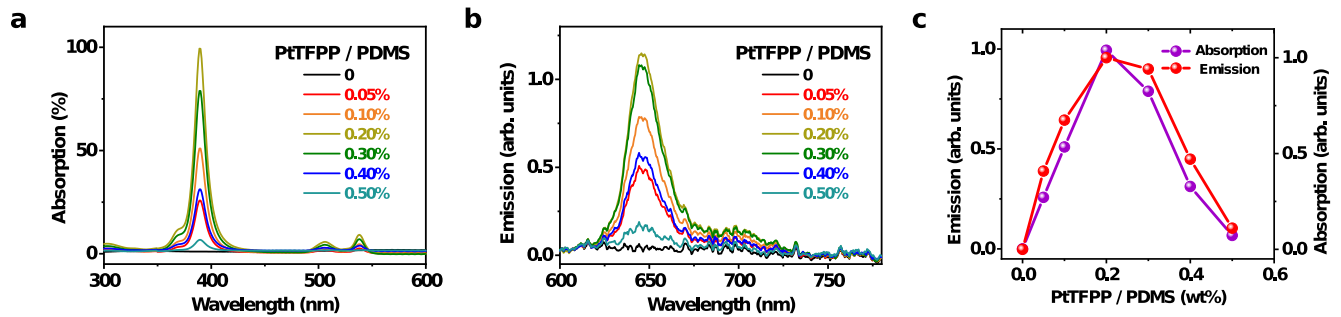
**Correspondence and requests for materials** should be addressed to He Ding, Guoguang Zhao or Xing Sheng.

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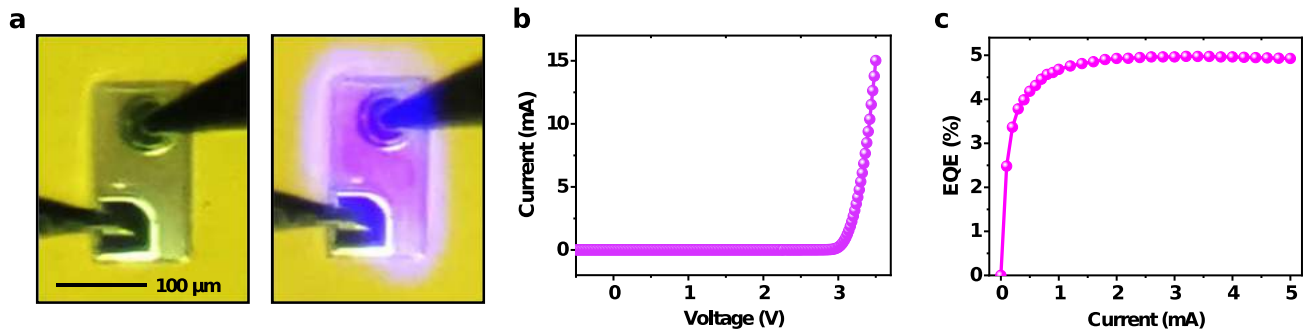
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**Extended Data Fig. 1** | Schematic illustration of the process flow for fabricating the  $p_{btO_2}$  sensing probe.

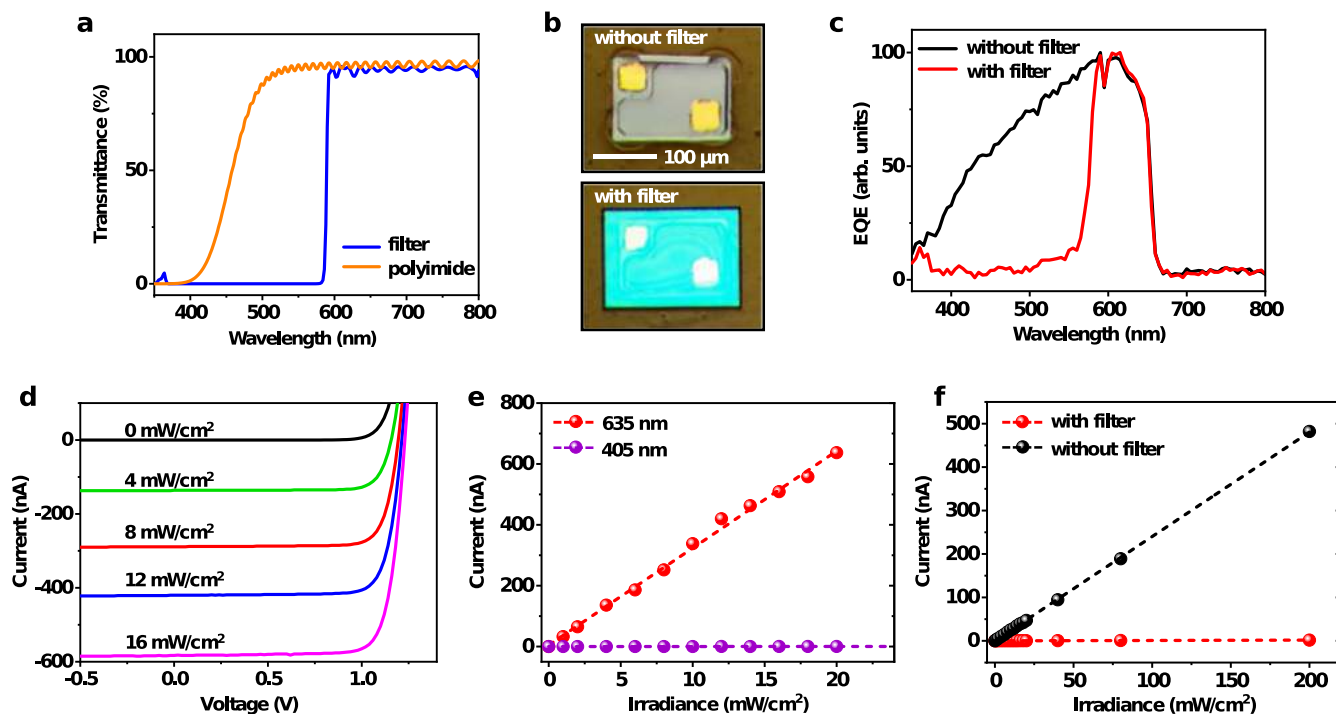


**Extended Data Fig. 2 | Optical properties of PtTFPP/PDMS films.** (a) Absorption and (b) PL emission spectra of PtTFPP with different mass concentrations mixed in PDMS films (thickness 10  $\mu\text{m}$ ). (c) Peak emissions and absorptions as a function of PtTFPP mass concentrations.



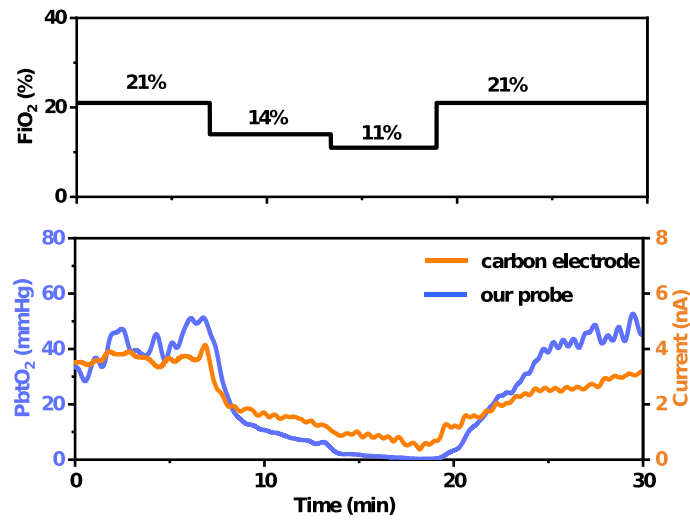
**Extended Data Fig. 3 | Images and optoelectronic properties of the InGaN violet LED.** (a) Microscopic images of a violet LED with (right) and without (left) electroluminescence. (b) The LED's current–voltage characteristic curve. (c) The LED's external quantum efficiencies (EQEs) as a function of currents.



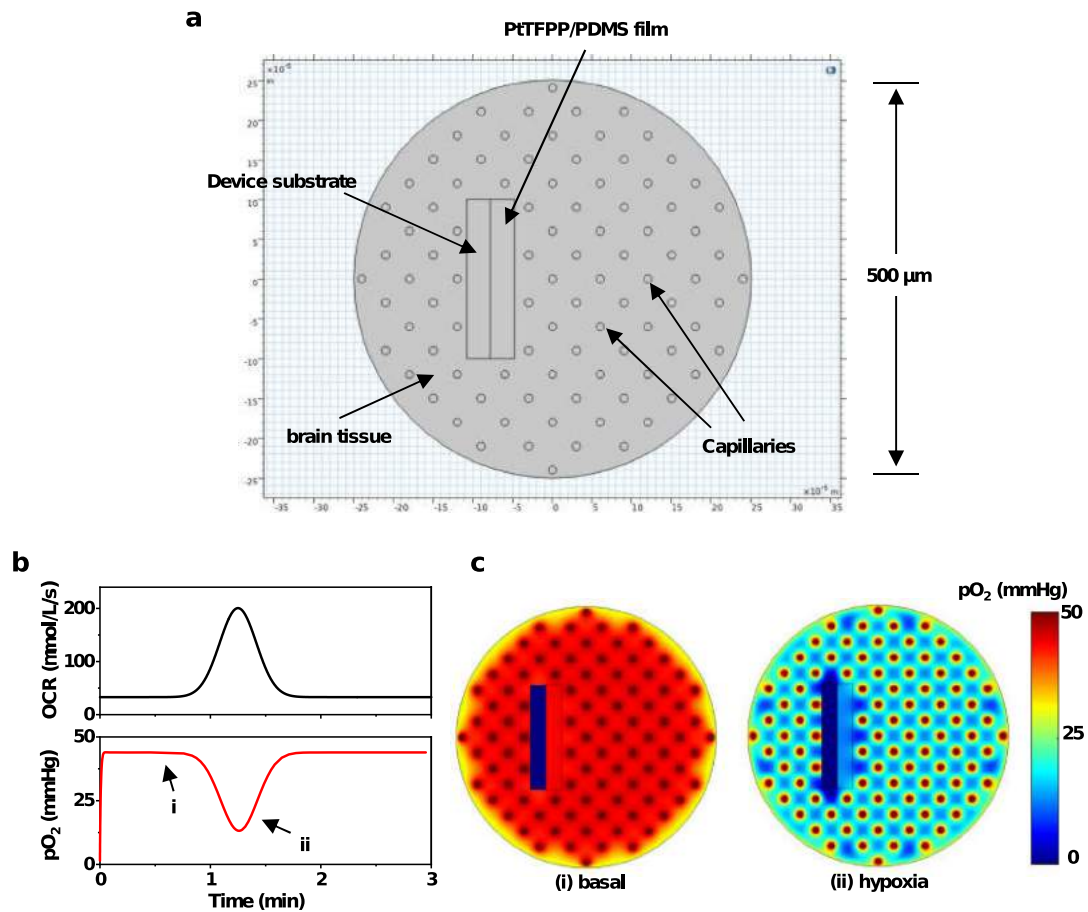


**Extended Data Fig. 4 | Images and optoelectronic properties of the InGaP photodetector.** (a) Transmission spectra of a polyimide film (thickness 8  $\mu\text{m}$ ) and a dielectric filter. (b) Images of InGaP detectors with (lower) and without (upper) the filter. (c) External quantum efficiency (EQE) spectra for InGaP detectors with and without coatings of polyimide and the filter. (d) Current-

voltage curves of an InGaP detector under different irradiances at 635 nm. (e) Photocurrent response of a detector coated with a filter measured at 405 nm and 635 nm illuminations. (f) Photocurrent response of a detector with and without filter coatings under 405 nm illumination.

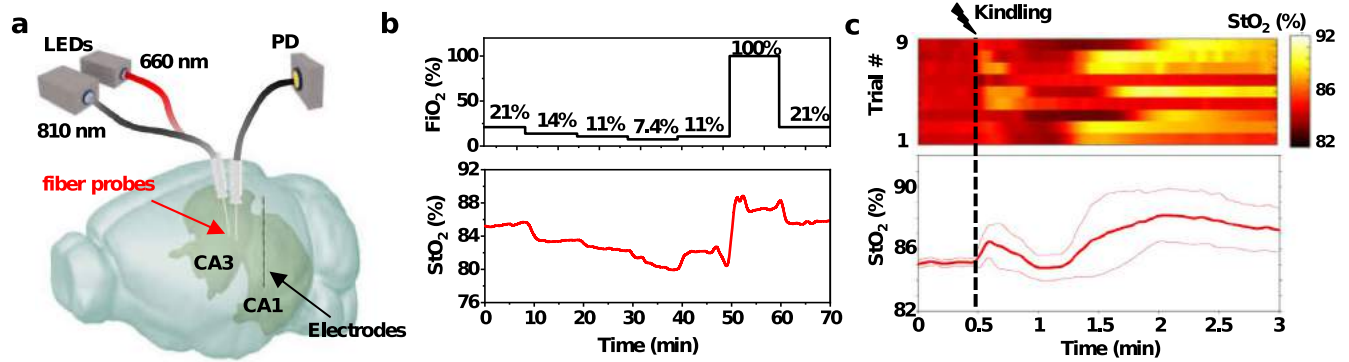


**Extended Data Fig. 5** | Dynamic change of  $F_{IO_2}$  (top) and  $p_{btO_2}$  results (bottom) recorded by our wireless micro-probe, in comparison with the data simultaneously detected by a carbon-based electrochemical electrode<sup>37</sup>.



**Extended Data Fig. 6 | Numerical simulation of  $\text{O}_2$  transport in brain tissue.** (a) 2D schematic model showing a PtTFPP/PDMS-based oxygen-sensitive film and capillaries within the brain tissue. (b) (top) Dynamic oxygen consumption

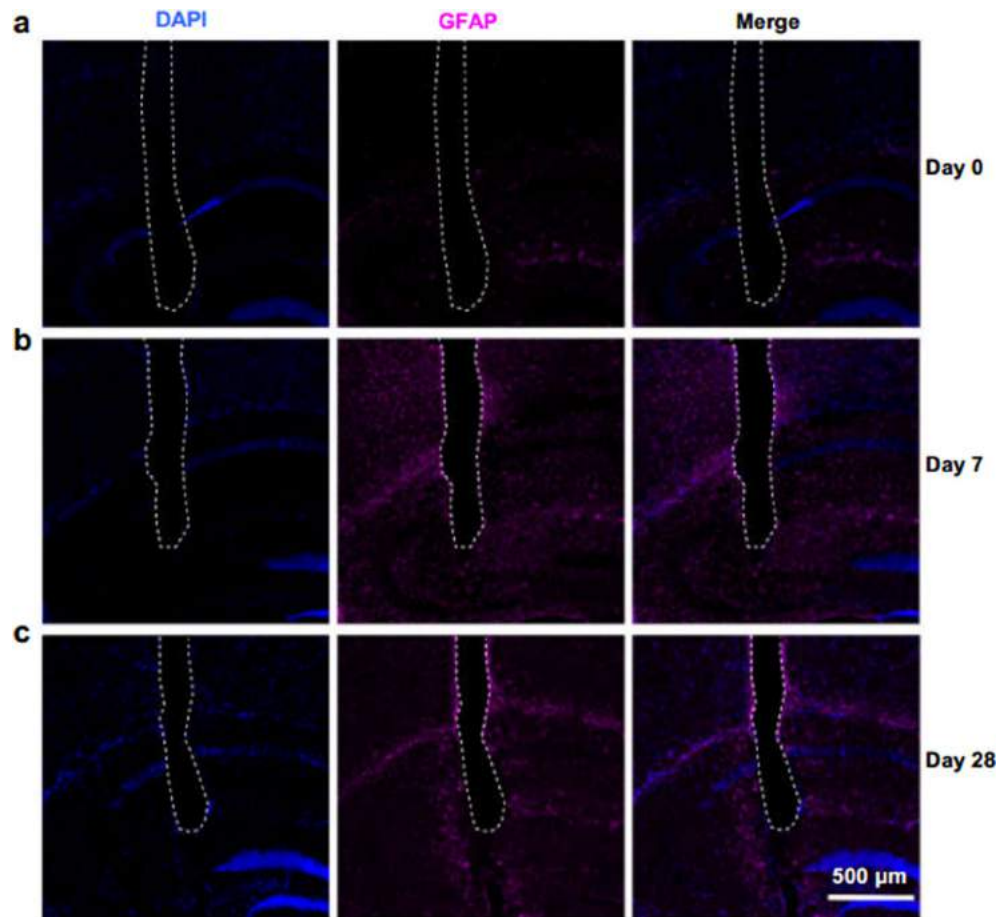
rate (OCR) imported into the model, and (bottom) the corresponding  $\text{O}_2$  pressure ( $p_{\text{O}_2}$ ) calculated in the PtTFPP/PDMS film. (c) Distributions of  $p_{\text{O}_2}$  in the tissue during (i) basal and (ii) hypoxia conditions.



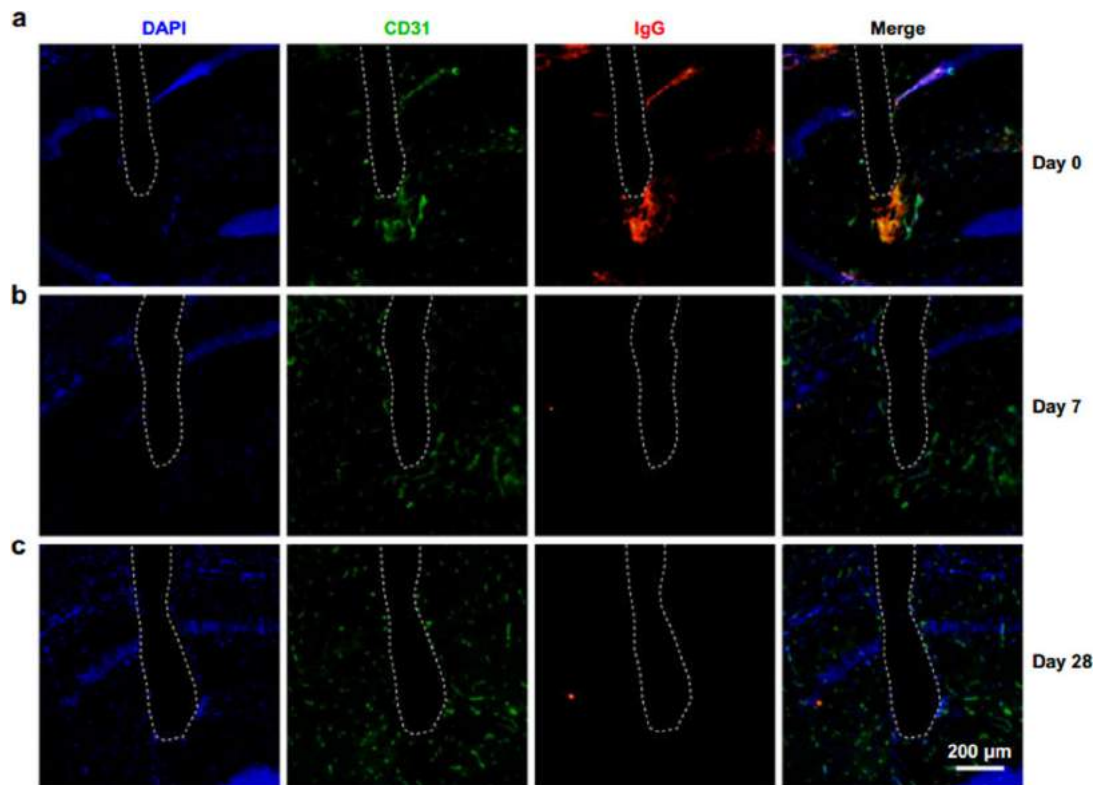
**Extended Data Fig. 7 | Measurement of tissue blood oxygen saturation ( $S_{tO_2}$ ) in the hippocampus of mice using a fibre-based setup.** (a) 3D schematic model showing positions of the two fibers and the stimulating electrode implanted in the ipsilateral hippocampus of mice (CA3 and CA1, respectively). One fiber couples to two LED sources emitting alternating red (660 nm) and infrared

(810 nm) light, and the other couples to a photodetector (PD). (b) Dynamic change of  $F_{iO_2}$  (top) and corresponding  $S_{tO_2}$  results (bottom). (c) Dynamic response of  $S_{tO_2}$  collected in CA3 immediately after kindling. Top: Heatmap of 9 individual trials from  $n = 3$  mice. Bottom: Average  $S_{tO_2}$  signals. The solid lines and shaded areas indicate the mean and s.e.m., respectively.





**Extended Data Fig. 8 | Representative confocal fluorescence images.** showing immunohistochemical staining for nuclei (DAPI, blue), astrocytes (GFAP, purple) and merged images after probe implantation for (a) 0, (b) 7 and (c) 28 days. Lesion areas are outlined by white dashed lines.



**Extended Data Fig. 9 | Representative confocal fluorescence images.** showing immunohistochemical staining for DAPI (blue), endothelial cells in blood vessels (CD31, green), immunoglobulin G (IgG, red) and merged images after probe implantation for (a) 0, (b) 7 and (c) 28 days. Lesion areas are outlined by white dashed lines.

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# A wireless optoelectronic probe to monitor oxygenation in deep brain tissue

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## Supplementary Information

### Preparation of individual components in the micro-probe

The layout of the microscale oxygen sensing probe includes (from top to bottom) a platinum(II)-5,10,15,20-tetrakis-(2,3,4,5,6-pentafluorophenyl)-porphyrin / poly(dimethylsiloxane) (PtTFPP/PDMS) sensing film (thickness:  $\sim 25 \mu\text{m}$ ), a PDMS/parylene C encapsulation layer (thickness:  $\sim 50 \mu\text{m}$ ), an SU-8 layer (thickness:  $5 \mu\text{m}$ ), an indium gallium nitride (InGaN) violet LED (size:  $190 \mu\text{m} \times 110 \mu\text{m} \times 10 \mu\text{m}$ ), a polyimide (PI) layer (thickness:  $8 \mu\text{m}$ ), an optical filter layer based on multilayer titanium dioxide ( $\text{TiO}_2$ ) and silicon dioxide ( $\text{SiO}_2$ ) (size:  $220 \mu\text{m} \times 150 \mu\text{m} \times 6 \mu\text{m}$ ), a PI layer (thickness:  $\sim 4 \mu\text{m}$ ) and an indium gallium phosphide (InGaP) photodetector (size:  $185 \mu\text{m} \times 125 \mu\text{m} \times 3 \mu\text{m}$ ), on a copper-clad PI film (Cu/PI/Cu:  $18/25/18 \mu\text{m}$ ). Contacts of the LED and the detector are metallized with sputtered metal layers (Cr/Au/Cu/Au =  $6 \text{ nm}/100 \text{ nm}/600 \text{ nm}/150 \text{ nm}$ ).

### Fabrication of InGaP detectors

The InGaP detector structure is grown on gallium arsenide (GaAs) substrates via metal-organic chemical vapor deposition (MOCVD). The epitaxially grown stack include (from top to bottom): a 500 nm n-type (Si-doped,  $2 \times 10^{18} \text{ cm}^{-3}$ )  $(\text{Al}_{0.7}\text{Ga}_{0.3})_{0.5}\text{In}_{0.5}\text{P}$  filter layer, a 10 nm n-type GaAs (Si-doped,  $>6 \times 10^{18} \text{ cm}^{-3}$ ) top contact layer, a 30 nm n-type (Si-doped,  $5 \times 10^{18} \text{ cm}^{-3}$ )  $\text{In}_{0.5}\text{Al}_{0.25}\text{Ga}_{0.25}\text{P}$  window layer, a 100 nm n-type (Si-doped,  $2 \times 10^{18} \text{ cm}^{-3}$ )  $\text{In}_{0.5}\text{Ga}_{0.5}\text{P}$  emitter layer, a  $1 \mu\text{m}$  p-type (Zn-doped,  $3 \times 10^{16} \text{ cm}^{-3}$ )  $\text{In}_{0.5}\text{Ga}_{0.5}\text{P}$  base layer, a 100 nm p-type (Mg-doped,  $2 \times 10^{18} \text{ cm}^{-3}$ )  $\text{In}_{0.5}\text{Al}_{0.25}\text{Ga}_{0.25}\text{P}$



back-surface field (BSF) layer, a 100 nm p-type (Mg-doped,  $>5 \times 10^{18} \text{ cm}^{-3}$ ) GaAs contact layer, a 1  $\mu\text{m}$  p-type  $\text{In}_{0.5}\text{Ga}_{0.5}\text{P}$  (Mg-doped,  $2 \times 10^{18} \text{ cm}^{-3}$ ) support layer and a 500 nm undoped  $\text{Al}_{0.95}\text{Ga}_{0.05}\text{As}$  sacrificial layer on a GaAs substrate (Table S1).

A detailed description of the process to fabricate the freestanding microscale photodetector is listed below:

1. Clean the epi-wafer with acetone, isopropyl alcohol (IPA), and deionized (DI) water.
2. Dehydrate at 110 °C for 15 min.
3. Spin coat positive photoresist (PR) (SPR220-v3.0, Microchem, 500 rpm / 6 s, 3000 rpm / 30 s) and soft-bake at 110 °C for 1.5 min.
4. Expose PR with a UV lithography tool (URE-2000/25, IOE CAS) with a dose of 300  $\text{mJ}/\text{cm}^2$  through a chrome mask, post-bake at 110 °C for 1.5 min.
5. Develop PR in an aqueous base developer (AZ300 MIF), rinse with DI water and hard-bake at 110 °C for 20 min.
6. Etch the  $(\text{Al}_{0.7}\text{Ga}_{0.3})_{0.5}\text{In}_{0.5}\text{P}$  filter with a mixture of  $\text{H}_3\text{PO}_4$  and  $\text{HCl}$  (1:1 by volume) for  $\sim 7$  s and rinse with DI water.
7. Etch the n-type GaAs contact and the  $\text{In}_{0.5}\text{Al}_{0.25}\text{Ga}_{0.25}\text{P}$  window with a mixture of  $\text{H}_3\text{PO}_4$ ,  $\text{H}_2\text{O}_2$ , and  $\text{H}_2\text{O}$  (3:1:25 by volume) for  $\sim 12$  s and rinse with DI water.
8. Remove the PR using acetone, IPA and DI water.
9. Dehydrate at 110 °C for 15 min.
10. Spin coat positive photoresist (PR) (SPR220-v3.0, Microchem, 500 rpm / 6 s, 3000 rpm / 30 s) and soft-bake at 110 °C for 1.5 min.

11. Expose PR with UV lithography tools (URE-2000/25, IOE CAS) with a dose of 300 mJ/cm<sup>2</sup> through a chrome mask and post-bake at 110 °C for 1.5 min.
12. Develop PR in aqueous base developer (AZ300 MIF), rinse with DI water and hard-bake at 110 °C for 20 min.
13. Etch the In<sub>0.5</sub>Ga<sub>0.5</sub>P emitter, the In<sub>0.5</sub>Ga<sub>0.5</sub>P base and the In<sub>0.5</sub>Al<sub>0.25</sub>Ga<sub>0.25</sub>P BSF with concentrated HCl for ~20 s.
14. Remove PR using acetone, IPA, DI water.
15. Dehydrate at 110 °C for 15 min.
16. Spin coat negative photoresist (AZ® nLOF 2070, MicroChemicals, 500 rpm / 6 s, 3000 rpm / 30 s) and soft-bake at 110 °C for 2 min.
17. Expose PR with UV lithography tools (URE-2000/25, IOE CAS) with a dose of 60 mJ/cm<sup>2</sup> through a chrome mask and post-bake at 110 °C for 75 s.
18. Develop PR in aqueous base developer (AZ300 MIF), rinse with DI water.
19. Sputter 6 nm/200 nm of Cr/Au.
20. Lift-off in acetone, and clean the wafer using acetone, IPA, DI water.
21. Dehydrate at 110 °C for 15 min.
22. Pattern PR (SPR220-3.0, Microchem).
23. Etch the p+ GaAs contact in a mixture of H<sub>3</sub>PO<sub>4</sub>/H<sub>2</sub>O<sub>2</sub>/H<sub>2</sub>O (3:1:25, by volume) for 40 s and rinse with DI water.
24. Etch the In<sub>0.5</sub>Ga<sub>0.5</sub>P support and the Al<sub>0.95</sub>Ga<sub>0.05</sub>As sacrificial layer with concentrated HCl for ~40 s.
25. Remove the PR using acetone, IPA, DI water.

26. Pattern PR (SPR220-3.0, Microchem).
27. Etch in diluted HF (49% HF : DI water = 1:10, by volume) to release the devices from GaAs growth substrates for ~2.5 h and rinse with DI water.
28. The free-standing InGaP photodetector arrays are formed and ready for picking up.

### *Fabrication of violet InGaN LEDs*

The InGaN based violet LED structures are grown on 2-inch planar sapphire substrates using MOCVD. The main LED structure (from bottom to top) includes: the sapphire substrate, a GaN buffer layer, an n-GaN, an InGaN / GaN multiple-quantum-well (MQW) layer, a p-GaN and an indium tin oxide (ITO) layer for top contacts. The thickness of the entire epitaxial structure is about 10  $\mu\text{m}$ . LED devices are lithographically fabricated, with Cr/Au layers serving as ohmic contacts. Inductively couple plasma reactive ion etching (ICP-RIE) is used to define the LED mesa (lateral dimension 190  $\mu\text{m}$   $\times$  110  $\mu\text{m}$ ). After bonding the fully fabricated LED arrays onto a thermal release tape (TRT) (Nitto Denko Corp.), laser lift-off (LLO) is applied to separate the thin-film LEDs from sapphire substrates by thermally decompose GaN into gallium (Ga) metal and nitrogen gas at the interface. A krypton fluoride (KrF) excimer laser at 248 nm (Coherent, Inc., CompexPro110) serves as the light source, with a uniform irradiation area of 5 mm  $\times$  15 mm. The power density during LLO is optimized to be around 0.6 J/cm<sup>2</sup> for LEDs. After laser irradiation, the micro-LEDs are released from sapphire by mild mechanical force at 70 °C (melting point of Ga is 29.7 °C). By

heating up to 120 °C, the LEDs are detached from the TRT (the critical release temperature is about 110 °C) and ready for transfer printing by PDMS.

#### *Fabrication of thin-film filters*

The filter structure is deposited on a GaAs substrate using ion beam-assisted sputter deposition. The multilayered structure consists of titanium dioxide (TiO<sub>2</sub>) and silicon dioxide (SiO<sub>2</sub>) films with a total thickness of about 6.6 μm. Its detailed layer structure can be found in our previous work<sup>1</sup>. Its shape (size: 220 μm × 150 μm) is defined through femtosecond laser-cutting (800 nm, Ti-sapphire laser system, Coherent Inc.). Subsequently, the GaAs substrate is removed in a mixed solution with NH<sub>4</sub>OH, H<sub>2</sub>O<sub>2</sub> and H<sub>2</sub>O (1:1:2, by volume) for ~8 hours. Finally, PDMS stamps (Sylgard 184 from Dow Corning) are utilized to transfer and print the freestanding thin-film filters onto other foreign substrates.

#### *Synthesis of the PtTFPP/PDMS film*

To fabricate the oxygen-sensitive film, commercial platinum(II)-5,10,15,20-tetrakis-(2,3,4,5,6-pentafluorophenyl)-porphyrin (PtTFPP) powders (PtT975, Frontier Scientific) are dissolved in toluene (0.08 mol/L), followed by the addition of the base component (part A) of polydimethylsiloxane (PDMS) to the solution, with different PtTFPP: PDMS weight ratios (0–0.50 wt%). After evaporating the solvent overnight, the substance is mixed with curing agent (part B) of PDMS with a weight ratio of 10:1

(part A/part B). Subsequently, vacuum evacuation removes air bubbles. The PtTFPP/PDMS film is ready for dip coating on the optoelectronic micro-probe.

*Preparation of the adhesive solution*

The adhesive solution comprises: bisphenol A glycerolate (1 glycerol/phenol) diacrylate, 3-(Trimethoxysilyl) propyl methacrylate, spin-on-glass (SOG 500F, Filmtronics Inc.), 2-Benzyl-2-(dimethylamino)-4'-morpholinobutyrophenone, and anhydrous ethanol<sup>2</sup>. The weight ratio is 200:100:100:9:2000. Stir at room temperature until full mixing. Store the mixed solution in refrigerator (4 °C) for future use.

## **Fabrication of the microscale optoelectronic probe**

A detailed description of the fabrication process is listed below:

### Substrate preparation

1. Cut the copper-clad PI substrate (Cu/PI/Cu: 18/25/18  $\mu\text{m}$ , DuPont) into small pieces (size: 15 mm  $\times$  18 mm).
2. Laminate the copper-clad polyimide film onto a PDMS coated glass slide
  - a. Degas PDMS (Sylgard 184) 10 : 1 (base: curing agent, by weight).
  - b. Spin cast PDMS to a glass slide at 500 rpm/6 s, 3000 rpm/30 s to form a PDMS film (thickness:  $\sim$ 10  $\mu\text{m}$ ).
  - c. Bake the glass for 23 s at 110  $^{\circ}\text{C}$ .
  - d. Laminate the PI film onto the PDMS coated glass. Make sure that the polyimide attaches to PDMS tightly without any bubbles.
  - e. Bake the sample for 30 mins at 110  $^{\circ}\text{C}$  until PDMS is fully cured.
  - f. Clean the sample by acetone, IPA and DI water.
  - g. Dehydrate at 110  $^{\circ}\text{C}$  for 15 min.
  - h. Spin cast 8  $\mu\text{m}$  polyimide (YDPI-102, Jing'ai Microelectronics) at 500 rpm/9 s, 3000 rpm/30 s to form an insulating film.
  - i. Bake the sample for 1 h at 80  $^{\circ}\text{C}$ , 1 h at 130  $^{\circ}\text{C}$ , 1 h at 180  $^{\circ}\text{C}$ , 3 h at 230  $^{\circ}\text{C}$ .

### InGaP detector transfer

3. Clean the PI sample by acetone, IPA and DI water.



4. Dehydrate at 110 °C for 15 min.
5. Spin coat negative photoresist (PR) (AZ nLOF 2070, 500 rpm / 6 s, 3000 rpm / 30 s) and soft-bake at 110 °C for 2 minutes 20 seconds.
6. Expose PR with UV lithography tools (URE-2000/25, IOE CAS) with a dose of 60 mJ/cm<sup>2</sup> (URE-2000/25, IOE CAS) through a chrome mask and post-exposure bake at 110 °C for 75 s.
7. Develop PR in an aqueous base developer (AZ300 MIF) and rinse with DI water.
8. Deposit 50 nm Al as the markers by sputtering.
9. Lift off PR in acetone.
10. Clean the substrate and dehydrate at 110 °C for 10 min.
11. Spin coat the prepared adhesive solution (500 rpm/6 s, 3000 rpm/30 s) on the substrate and soft-bake at 110 °C for 3 mins.
12. Transfer print InGaP detectors from the source GaAs wafer onto the processed substrate with PDMS stamps.
13. Cure under UV for 10 minutes and bake at 110 °C for 3 h.
14. Clean the PR by reactive ion etching (RIE) (O<sub>2</sub>, 200 sccm, 90 mTorr, 150 W) for 12 min.

#### *InGaP detector encapsulation*

15. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
16. Clean by RIE (O<sub>2</sub>, 200 sccm, 90 mTorr, 150 W) for 1 min.
17. Spin coat SU8-3005 epoxy (500 rpm/6 s, 3000 rpm/30 s).
18. Soft-bake at 65 °C for 1 min and 95 °C for 3 min.

19. Pattern SU8 to expose contact pads of the detector by UV lithography with a dose of 210 mJ/cm<sup>2</sup>.
20. Post-bake at 65 °C for 1 min and 95 °C for 2 min.
21. Develop in propylene glycol monomethyl ether acetate (PGMEA) for 2.5 min and rinse with IPA.
22. Hard bake at 130 °C for 2h.

#### *InGaP detector metallization*

23. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
24. Pattern PR AZ nLOF 2070.
25. Deposit Cr/Au/Cu/Au = 6 nm/100 nm/600 nm/150 nm by sputtering.
26. Lift-off PR in acetone.

#### *Filter transfer*

27. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
28. Spin coat 2 µm polyimide (500 rpm/6 s, 3000 rpm/30 s) and bake at 110 °C for 2 h.
29. Spin coat 2 µm polyimide (500 rpm/6 s, 3000 rpm/30 s).
30. Bake at 85 °C for 10 s.
31. Transfer print dielectric filters on top of detectors with PDMS stamps.
32. Hard-bake at 110 °C for 2 h.

#### *InGaN LED transfer*

33. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
34. Spin coat 8 µm polyimide (500 rpm/6 s, 3000 rpm/30 s).

35. Bake at 85 °C for 2 min.
36. Transfer print InGaN violet LEDs onto the substrate with PDMS stamps.
37. Hard-bake at 85 °C for 1 h and 130 °C for 4 h.

#### InGaN LED encapsulation

38. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
39. Clean by RIE (O<sub>2</sub>, 200 sccm, 90 mTorr, 150 W) for 1 min.
40. Spin coat SU8-3005 epoxy (500 rpm/6 s, 3000 rpm/30 s).
41. Soft-bake at 65 °C for 1 min and 95 °C for 3 min.
42. Pattern SU8 to expose contact pads of the LED by UV lithography with a dose of 210 mJ/cm<sup>2</sup>.
43. Post-bake at 65 °C for 1 min and 95 °C for 2 min.
44. Develop in PGMEA for 2.5 min and rinse with IPA.
45. Hard bake at 130 °C for 2h.

#### InGaN LED metallization

46. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
47. Pattern PR AZ nLOF 2070.
48. Deposit Cr/Au/Cu/Au = 6 nm/100 nm/600 nm/150 nm by sputtering.
49. Lift-off PR in acetone.

#### Device encapsulation

50. Clean the sample (acetone, IPA, DI water) and dehydrate at 110 °C for 15 min.
51. Expose under ultraviolet induced ozone (UV Ozone, PCE-22-LD, YIMA) for 15 min.

52. Pattern SU8-3005 epoxy (500 rpm / 5 s, 3000 rpm / 30 s), cure under UV for 210 mJ / cm<sup>2</sup> and bake at 110 °C for 30 min.

Laser milling

53. Use laser milling to cut the PI film into micro-probe shapes (LPKF ProtoLaser U4, 365 nm; 1000 Hz, 0.5 W, 50 repeats + 1 W, 100 repeats + 2W, 40 repeats)

Device encapsulation

54. Expose the micro-probes under UV ozone for 15 min.

55. Encapsulate the micro-probes with PDMS

- a. Degas PDMS 10:1 (base: curing agent, by weight).
- b. Dip coat the micro-probes with PDMS.
- c. Bake the probes in 75 °C for 2 h.

56. Coat the probes with a layer of parylene C (14 μm, Specialty Coating Systems).

57. Clean the probes with RIE (O<sub>2</sub>, 200 sccm, 90 mTorr, 150 W) for 1 min.

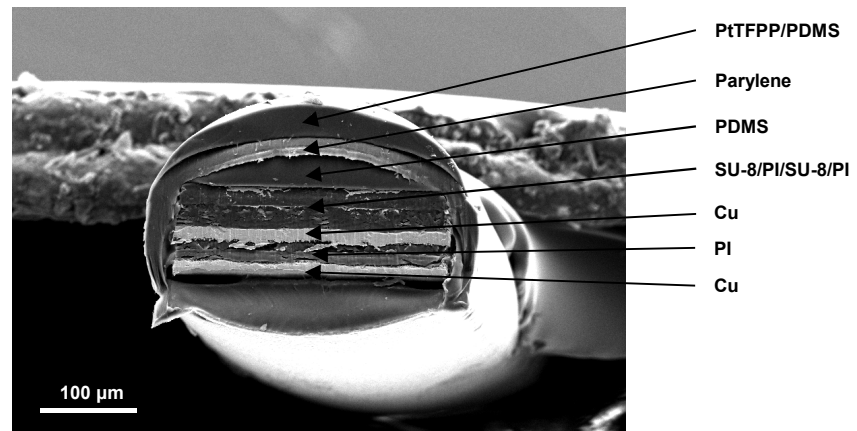
58. Encapsulate the probes with another layer of PDMS.

59. Dip the synthesized PtTFPP/PDMS on the tip of the probe.

## References

1. Li L, Tang G, Shi Z, Ding H, Liu C, Cheng D, et al. Transfer-printed, tandem microscale light-emitting diodes for full-color displays. *Proceedings of the National Academy of Sciences* 2021, 118(18): e2023436118.
2. Kim T-i, Kim MJ, Jung YH, Jang H, Dagdeviren C, Pao HA, et al. Thin film receiver materials for deterministic assembly by transfer printing. *Chemistry of Materials* 2014, 26(11): 3502-3507.

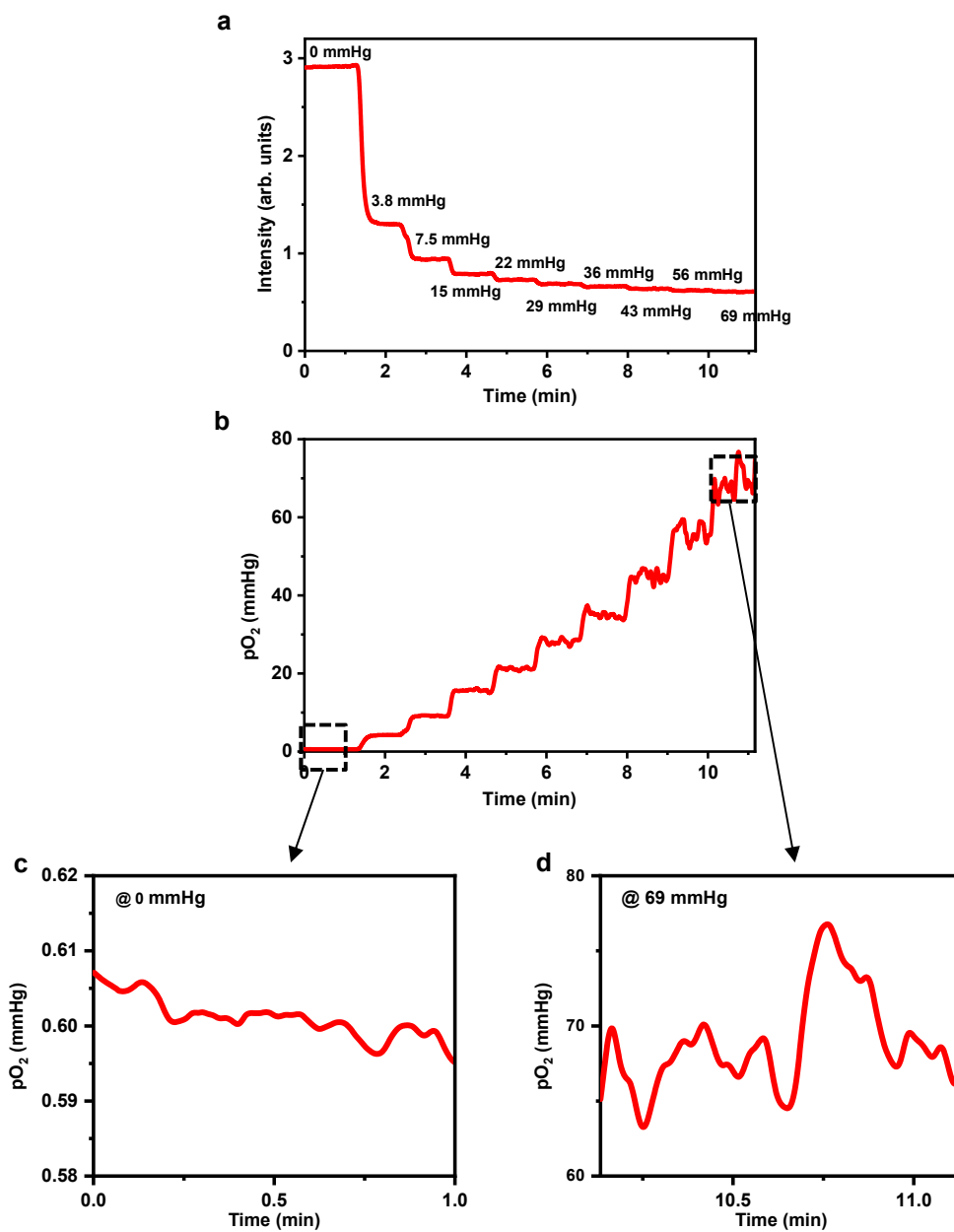
## Figure S1



**Figure S1.** SEM image (cross-sectional view) of the probe with encapsulation layers.

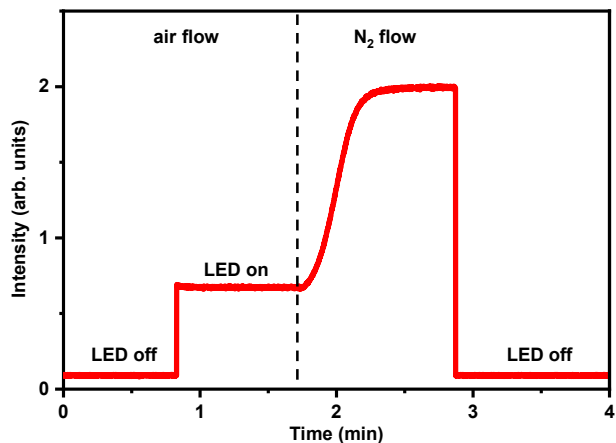


## Figure S2



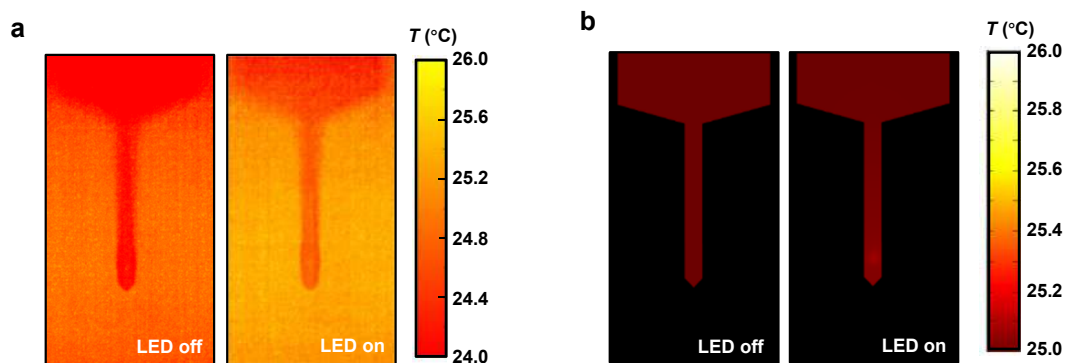
**Figure S2.** (a) Recorded PL intensities at different O<sub>2</sub> partial pressures changing with time. (b) Calibrated O<sub>2</sub> partial pressures with time based on the Stern-Volmer equation. (c, d) Partially enlarged curve of (b) at (c) 0 mmHg and (d) 69 mmHg.

### Figure S3



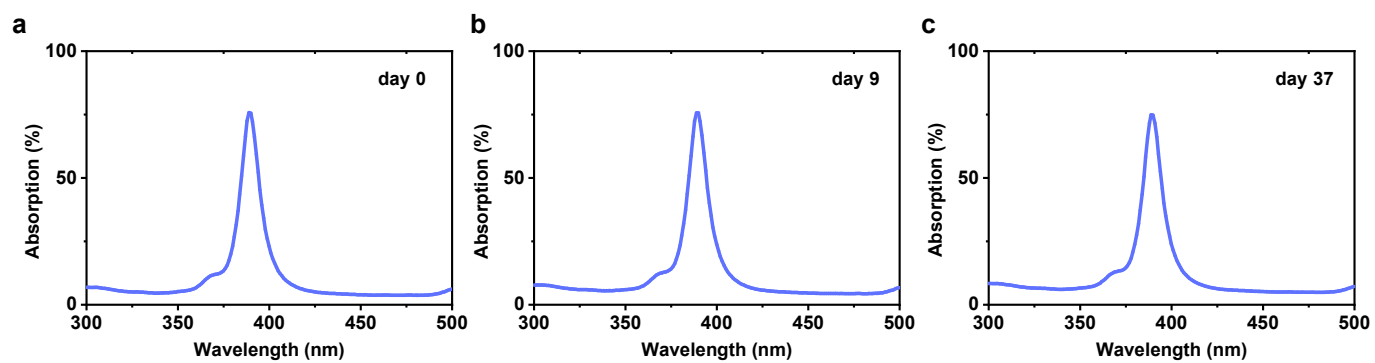
**Figure S3. Composition of the recorded signal.** The initial value of the signal collected by the circuit is set to 0.1 to enable the amplifier to operate within its linear range. When the LED is on, the signal in air (~0.5) mainly comes from the excitation violet light, which cannot be completely blocked by the filter and leaks into the detector. When N<sub>2</sub> is filled into the chamber, phosphorescence becomes stronger, which can be used to calculate PbO<sub>2</sub>.

## Figure S4



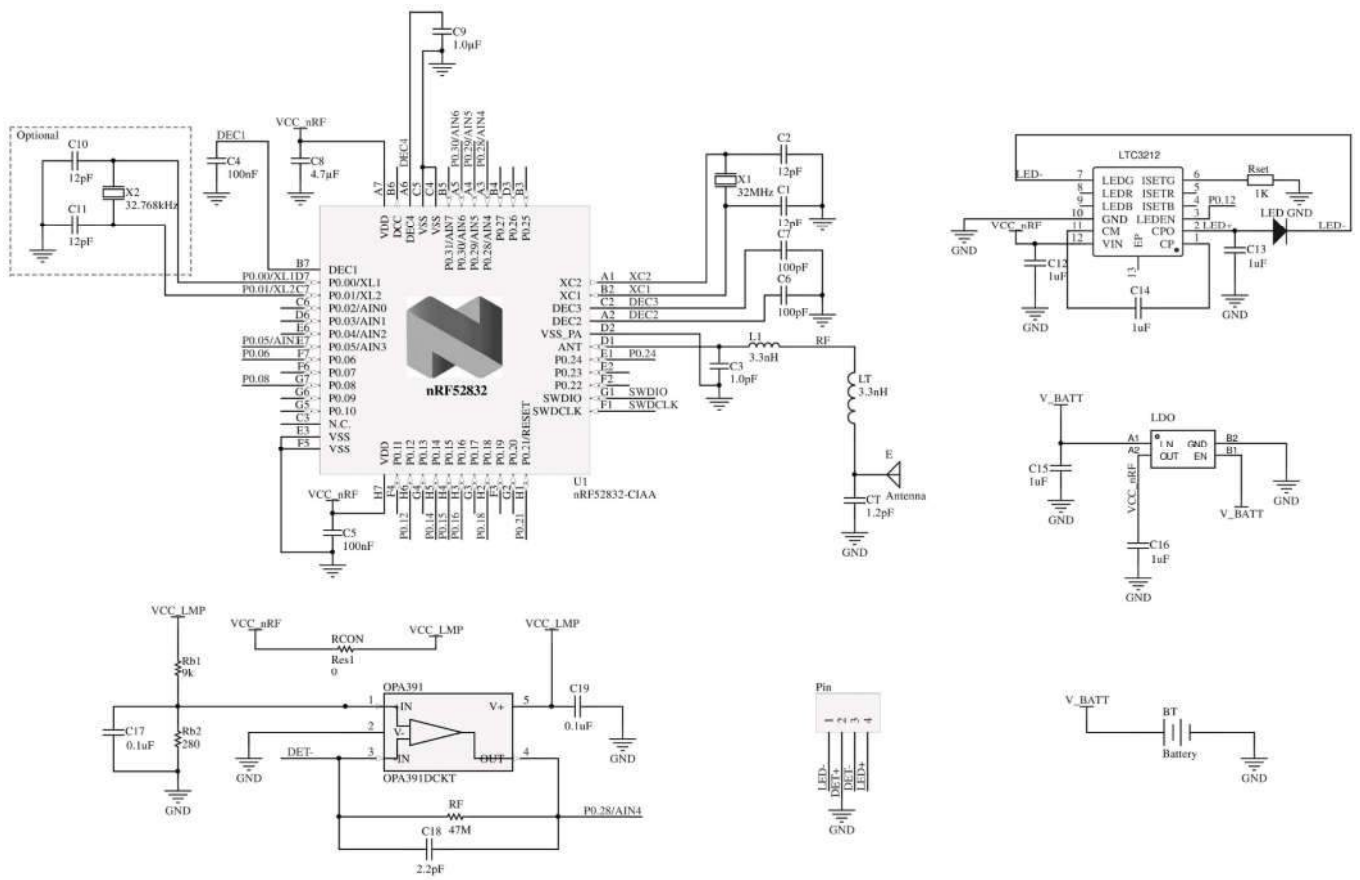
**Figure S4. Thermal properties of the probe.** (a) Measured and (b) simulated temperature distributions on the probe surface when the violet LED is off (left) or on (right) in air (LED current 0.5 mA, frequency 4 Hz, duty cycle 5%).

## Figure S5



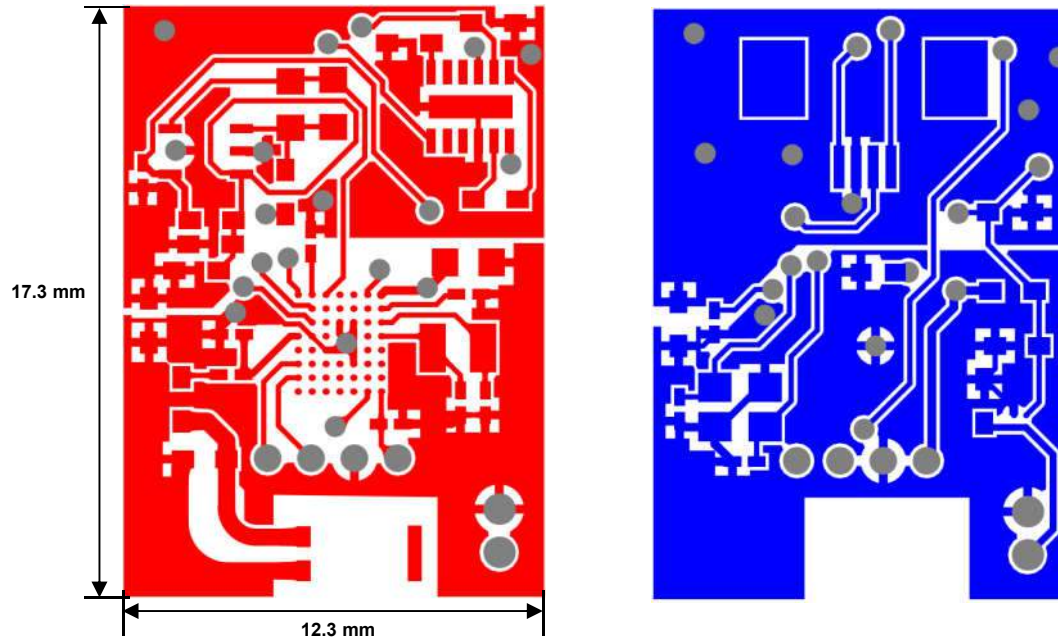
**Figure S5.** Absorption spectra of the oxygen sensing film immersing the film in PBS for 0 day (a), 9 days (b) and 37 days (c).

**Figure S6**



**Figure S6.** Detailed circuit design diagram of the wireless circuit system.

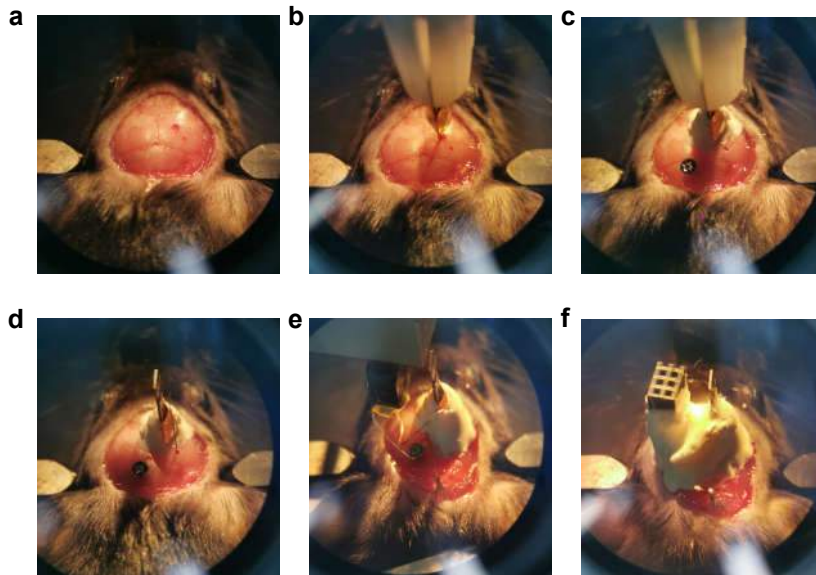
**Figure S7**



**Figure S7.** Layout of the designed printed circuit board for the wireless, battery-powered circuit system (red, top layer; blue, bottom layer).

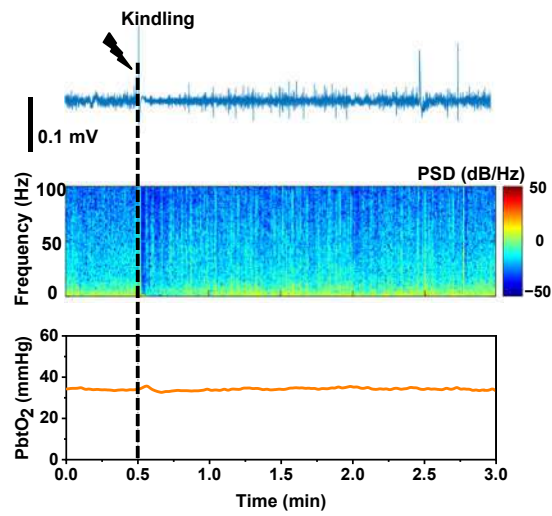


## Figure S8



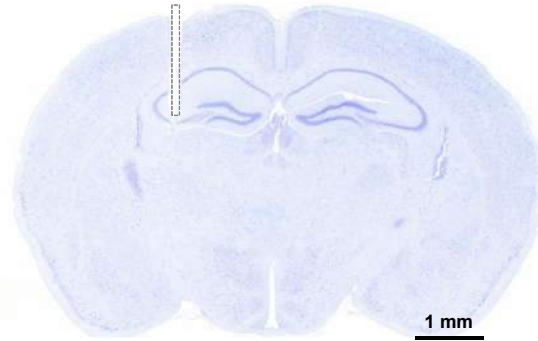
**Figure S8. Photographs showing the surgical procedure of implanting a PbtO<sub>2</sub> sensing probe as well as recording and stimulation electrodes into the mouse hippocampus.** (a) Expose the skull, and drill a hole on the skull. (b) Implant the probe into mouse brain. (c) Apply dental cements to fix the probe to the skull, and implant a screw as a reference electrode. (d) Implant stimulation and recording electrodes into the brain. (e) Fix the electrodes with dental cements. (f) Wire the electrodes to a connector, and apply more dental cements to fix all components.

## Figure S9



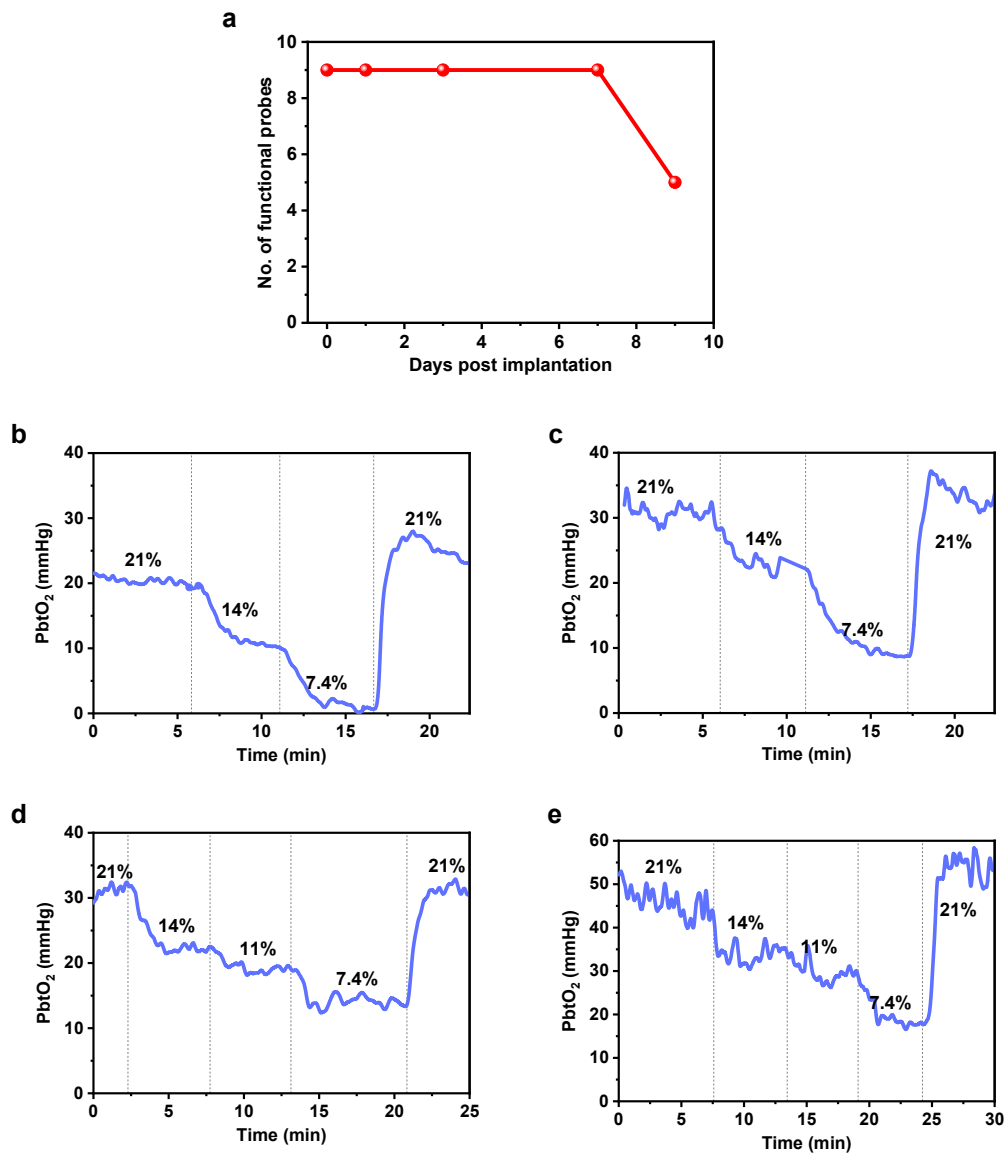
**Figure S9.** Simultaneously recorded electrophysiological activities in CA1 and PbtO<sub>2</sub> in CA3 under kindling from a mouse without afterdischarge. Top: LFP trace. Middle: power spectral density (PSD) of LFP. Bottom: PbtO<sub>2</sub>.

## Figure S10



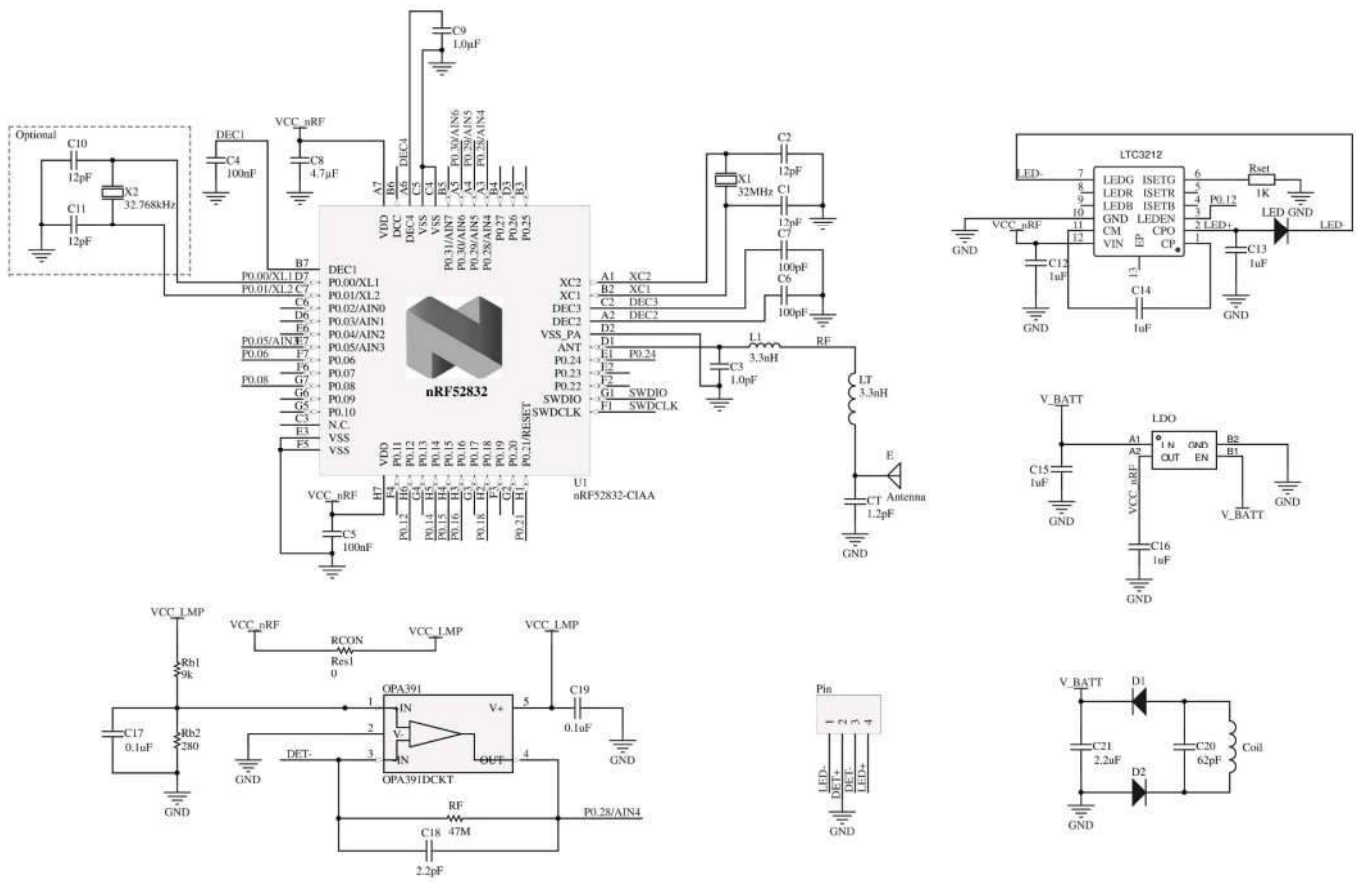
**Figure S10.** Coronal section stained with Nissl, showing the lesion region in the hippocampus (CA3) of mice created by the probe.

# Figure S11



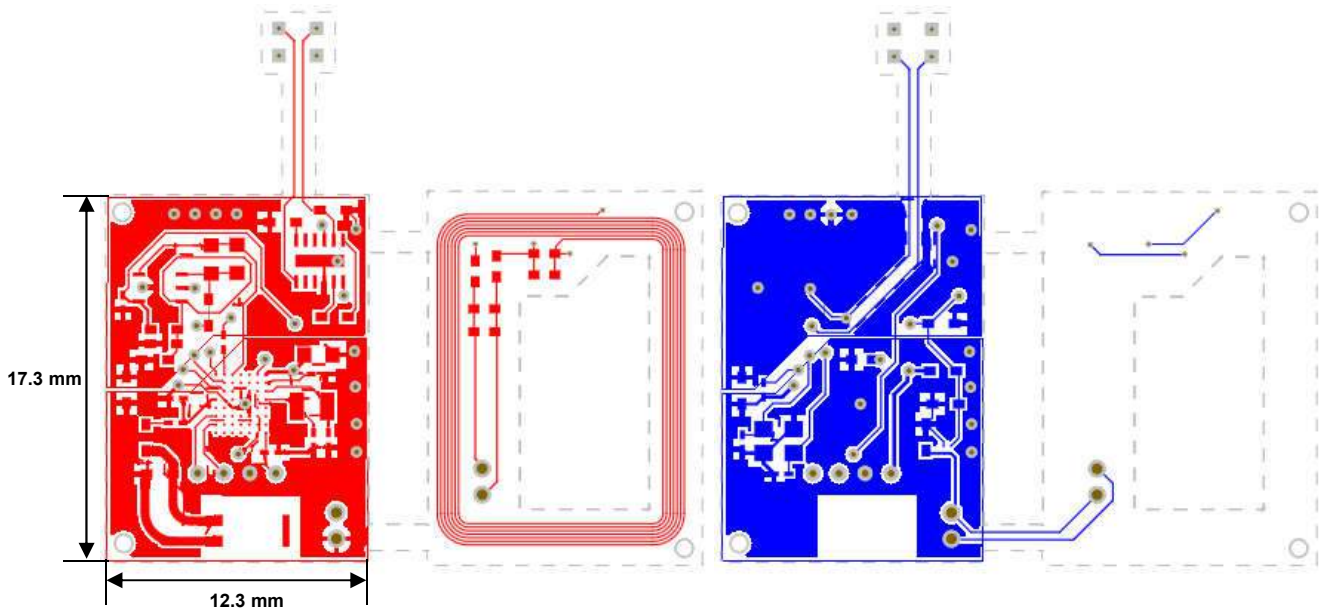
**Figure S11.** (a) Chronic stability of the implant probes. 9 probes are separately implanted into 9 behaving mice. Recorded PbtO<sub>2</sub> from a representative probe with changed FiO<sub>2</sub> after implantation for (b)1, (c) 3, (d) 7, and (e) 9 days.

**Figure S12**



**Figure S12.** Detailed circuit design diagram of the wireless, battery-free circuit system.

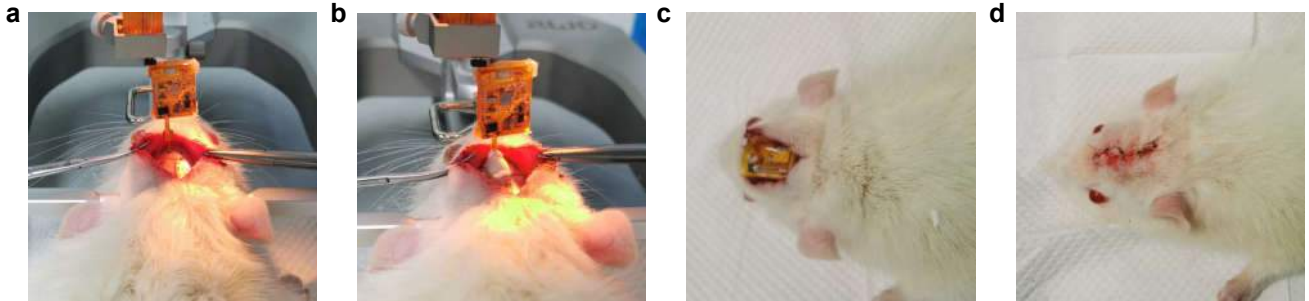
**Figure S13**



**Figure S13.** Layout of the designed printed battery-free circuit board for the wireless, battery-free circuit system (red, top layer; blue, bottom layer).

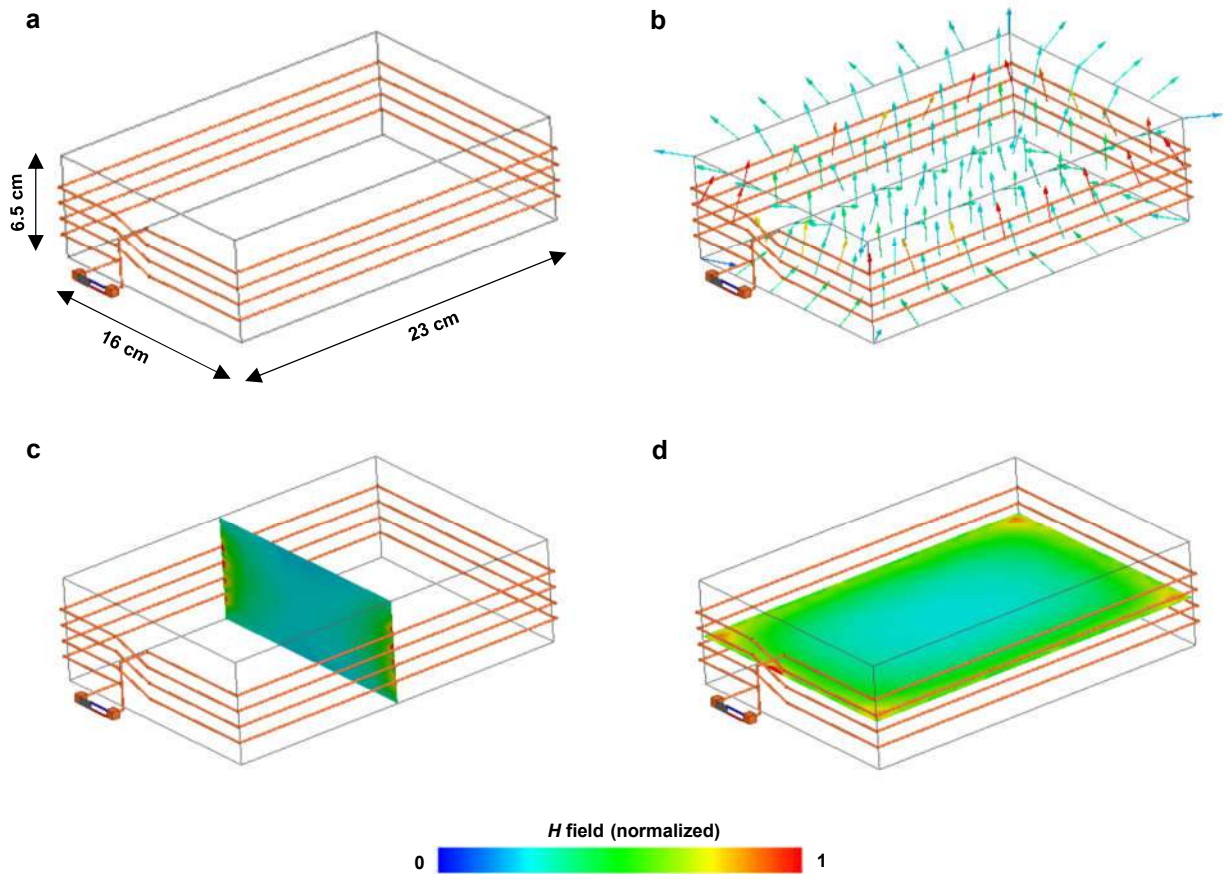


## Figure S14



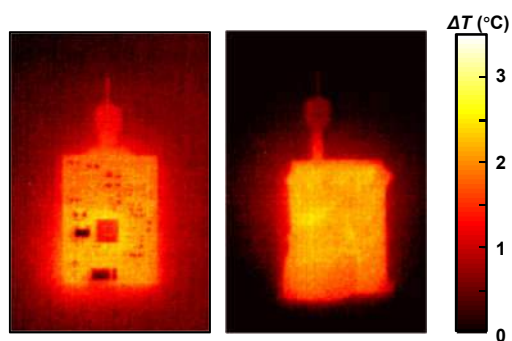
**Figure S14. Photographs showing the surgical procedure of implanting a probe and its associated battery-free circuit in a rat.** (a) Expose the skull, drill a hole on the skull and implant the probe into the rat brain. (b) Apply the dental cement to fix the probe to the skull. (c) Place the circuit underneath the skin. (d) Suture the skin.

**Figure S15**



**Figure S15.** (a) Schematic illustration of the antenna system for wireless power transfer (dimension:  $W \times L \times H = 16\text{ cm} \times 23\text{ cm} \times 6.5\text{ cm}$ ). (b) Simulated magnetic field distribution (normalized) inside the box. (c) Longitudinal and (d) Cross-sectional view of the field distribution.

## Figure S16



**Figure S16. Thermal properties of wireless circuits.** (a) Battery-powered circuit. (b) Inductively powered, battery-free circuit (coated with PDMS).

# Table S1

| Materials               | Thickness (nm) |
|-------------------------|----------------|
| ITO                     | 150            |
| p+ GaN                  | 150            |
| Electron blocking layer | 50             |
| MQWs                    | 140            |
| n+ GaN                  | 3000           |
| U GaN                   | 5800           |
| sapphire substrate      | -              |

**Table S1.** Epitaxial structure of the InGaN violet LED wafer.

**Table S2**

| Materials   | Thickness (nm) | Doping (cm <sup>-3</sup> ) | Dopant |
|---|----------------|----------------------------|--------|
| n+ In <sub>0.5</sub> Al <sub>0.7</sub> Ga <sub>0.3</sub> P filter   | 500            | 2e18                       | Si     |
| n+ GaAs contact   | 10             | >6e18                      | Si     |
| n+ In <sub>0.5</sub> Al <sub>0.25</sub> Ga <sub>0.25</sub> P window | 30             | 5e18                       | Si     |
| n+ In <sub>0.5</sub> Ga <sub>0.5</sub> P emitter                    | 100            | 2e18                       | Si     |
| p In <sub>0.5</sub> Ga <sub>0.5</sub> P base                        | 1000           | 3e16                       | Zn     |
| p+ In <sub>0.5</sub> Al <sub>0.25</sub> Ga <sub>0.25</sub> P BSF    | 100            | 2e18                       | Mg     |
| p+ GaAs contact   | 100            | >5e18                      | Mg     |
| p+ In <sub>0.5</sub> Ga <sub>0.5</sub> P support                    | 1000           | 2e18                       | Mg     |
| Al <sub>0.95</sub> Ga <sub>0.05</sub> As sacrificial                | 500            | undoped                    | -      |
| GaAs substrate  | -              | -                          | -      |

**Table S2.** Epitaxial structure of the InGaP based detector wafer.

**Table S3**

| Symbol                  | Component  | Package  |
|-------------------------|--|--|
| RJ, RCON, RG2, RG1      | Resistor, 0 $\Omega$   | R0402  |
| RF                      | Resistor, 100 M $\Omega$   | R0603  |
| R1                      | Resistor, 280 $\Omega$   | R0402  |
| R2                      | Resistor, 9 k $\Omega$   | R0402  |
| C19                     | Capacitor, 0.1 $\mu$ F, NP0                                      | C0201  |
| C12, C13, C14, C15, C16 | Capacitor, 1 $\mu$ F, NP0  | C0402  |
| C18                     | Capacitor, 2.2 pF, NP0   | C0603  |
| C17                     | Capacitor, 0.1 $\mu$ F, NP0                                      | C0402  |
| LDO                     | NCP161AFCS330T2G   | WCSP (4)   |
| OPA391                  | OPA391DCKR   | SC70 (5)   |
| BT                      | XH-2A  | $P = 1.25$ mm                                      |
| Pin                     | F0502-B-04-20T-R   | SMD, $P = 0.5$ mm                                  |
| LTC3212                 | LTC3212EDDB  | 12-LEAD (3 $\times$ 2) mm                          |
| C1, C2, C10, C11        | Capacitor, 12 pF, NP0  | C0201  |
| C3                      | Capacitor, 1.0 pF, NP0   | C0201  |
| C4, C5                  | Capacitor, 100 nF, X7R   | C0201  |
| C6, C7                  | Capacitor, 100 pF, NP0   | C0201  |
| C8                      | Capacitor, 4.7 $\mu$ F, X5R                                      | C0603  |
| C9                      | Capacitor, 1.0 $\mu$ F, X5R                                      | C0402  |
| L1                      | Inductor, 3.3 nH   | L0201  |
| U1                      | nRF52832-CIAA  | WLCSP_C50  |
| X1                      | XTAL SMD 2016, 32 MHz,<br>CI = 8 pF, Total Tol: $\pm$ 40 ppm     | XTAL_2016  |
| X2                      | XTAL SMD 2012, 32.768 kHz,<br>CI = 9 pF, Total Tol: $\pm$ 50 ppm | XTAL_2012  |
| CT                      | Capacitor, 1.2 $\mu$ F, NP0                                      | C0402  |
| LT                      | Inductor, 3.3 nH   | L0402  |
| E                       | H2U34WGTQW0100   | SMD, 3.2 $\times$ 1.6 $\times$ 1.2 mm <sup>3</sup> |
| C20                     | Capacitor, 62 pF, NP0  | C0402  |
| C21                     | Capacitor, 2.2 $\mu$ F, NP0                                      | C0402  |
| D1, D2                  | Schottky diode   | DFN1006  |
| Battery                 | Rechargeable lithium ion battery<br>3.7 V, 45 mAh                | -  |

**Table S3.** List of components used in the wireless circuit systems powered by a battery or an RF coil.

## Table S4

| Ref.      | Monitoring target | Operational principle                         | Monitored body part | Cross-sectional area of the probe | Temporal response          | Resolution/Sensitivity                    | Device weight                     |
|-----------|-------------------|---|---------------------|-----------------------------------|----------------------------|---|-----------------------------------|
| 1         | oxygen saturation | Optical absorption of HbO <sub>2</sub> and Hb | Brains of rodents   | 400 × 200 μm <sup>2</sup>         | ~ 0.6 ms (pulse frequency) | 7%  | 0.083 g                           |
| 2         | oxygen saturation | Optical absorption of HbO <sub>2</sub> and Hb | Brains of rodents   | 600 × 160 μm <sup>2</sup>         | < 0.1 s (pulse frequency)  | 2.9%                                      | Wired                             |
| 3         | oxygen pressure   | Electro chemical                              | Muscles of rabbits  | 500 μm in diameter                | 20 s                       | -2.496 nA/mm Hg                           | Wired                             |
| 4         | oxygen pressure   | Electro chemical                              | Brains of rodents   | 180 μm in diameter                | < 1 s                      | 183 ± 14 pA/μM                            | 9.6 g                             |
| 5         | oxygen pressure   | Electro chemical                              | Lungs of sheep      | 2.8 × 1.4 mm <sup>2</sup>         | < 1 s                      | -0.595 ± 0.009 nA/kPa                     | Wired                             |
| 6         | oxygen pressure   | Electro chemical                              | Brains of rodents   | 7 μm in diameter                  | 5.99 ~ 8.04 s              | 0.85 ± 0.04 nA/μM                         | Wired                             |
| 7         | oxygen pressure   | PL quenching                                  | Kidneys of rodents  | 3 mm in diameter                  | < 5 min                    | –   | Wired                             |
| 8         | oxygen pressure   | PL quenching                                  | Muscles of sheep    | 3 × 4.5 × 1.2 mm <sup>3</sup>     | ~210 s                     | ~0.3 %/mm Hg at pO <sub>2</sub> = 10 mmHg | ~0.0174 g                         |
| 9         | oxygen pressure   | PL quenching                                  | –                   | 420 μm in diameter                | ~6 s                       | ~0.02 mmHg at pO <sub>2</sub> = 7.6 mmHg  | Wired                             |
| This work | oxygen pressure   | PL quenching                                  | Brains of rodents   | 330 × 200 μm <sup>2</sup>         | 0.9 s                      | < 0.8 mmHg at pO <sub>2</sub> = 3.8 mmHg  | 1.8 g /0.8 g (w/ and w/o battery) |

**Table S4.** Comparing characteristic parameters of wireless and wired implantable oxygenation sensors reported in the literature and this work.

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